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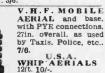


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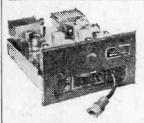
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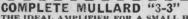
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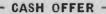
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A small versatile Unit employing the new MULLARD ECL86 valve and designed to provide two (or three) way conversation up to extreme distances. Operates from A.C. mains 200 to 250 Volts.

PRICES . . . MASTER UNIT and ONE EXTENSION

KIT OF PARTS £6.17.6 ASSEMBLED AND TESTED £8.0.0

Consists of a MASTER UNIT, size only 8½ x 5½ x 6in, and ONE EX-TENSION (a second extension may be added to any time). The Master Unit incorporates switching and power supply and with the chassis completely isolated from the mains is operated in absolute safety. Cases covered in quality leatherette.



| COLLARO "JUNIOR" 4 SPEED SINGLE RECORD PLAYER £3.15.0

with separate CRYSTAL PICK-UP £3.1
Carriage and Insurance 5/-.

Above PICK-UP separately for£1.6.8

PRICE REDUCTIONS

H.P. Terms: Deposit £5, 12 months of £1,16.8.

(c) kIT OF PARTS to build Two "5-10" MAIN AMPLIFIERS (Incorporating Parmeko Output Transformers) and the DUAL-CHANNEL PRE-AMPLIFIER CONTROL £31.0.0 UNIT (h) TWO "5-10" AMPLIFIERS and the DUAL-CHANNEL PRE-AMPLIFIER CONTROL UNIT BOTH £36.0.0 H.P. Terms: Deposit £7.4.0,112 months £2,12.0.

H.P. Terms: Deposit \$7.4.0.112 months \$2.12.0. Carriage and Insurance 7/6 extra. Prices quoted are subject to \$1.6.0 extra for Partridge Transformer.

DUAL CHANNEL PRE-AMP

Incorporates two Mullard 2-valve Pre-Amplifiers combined into a Single unit ena-blue tro he used for h 1) in 12. 10 (1)

and a PARMEKO blue to be used for both STEREOPHONIC or MONAURAL operation. It is designed primarily to operate with our range of MULLARD MAIN AMPLIFIERS but will also operate goully well with any make of Amplifiers requiring an input of 250 m/rolts.

COMPLETE KIT \$12.10.0 ASSEMBLED \$15.0.0

E KIT £12.10.0 ASSEMBLED AND TESTED #15.0.0

MULLARD FOUR CHANNEL MIXER UNIT

with Cathode powered Self powered with Cathode rollower output. Incorporates Two inputs for MICROPHONES One for CRYSTAL PICK UP and a fourth for RADIO or TAPE Complete Kit of Parts \$8.8.0

Assembled and Tested £10.0.0
TERMMS: Deposit £2 and £2 months at 15/MODEL I.L. one microphone input matched for moving coil or
Ribbon Mike. £1.17.0 extra.

RECORD PLAYERS THE LATEST MODELS ARE IN STOCK'
SEND S.A.E. FOR ILLUSTRATED LEAFLET
B.S.R. MONARCH UA8 4-speed mixer Autochanser
£6.19.8 £9.18.9

with Crystal Pick-up.
The NEW COLLARO MODEL RP594 4-speed Single
Record Player, Studio Cartridge. ord Player. Studio Cartridge.
NEW COLLARO Co 4-speed Autochanger unit
1 Studio "O" Pick-up. £7.19.6 vith Studio "O" Pick-up. The E.M. I. 4-speed Single Record Player with crystal with Studio £6.9.6

Pick-up.

8.S.R. MODELS UA12 and UA14. Each a 4-speed fixer autochanger with Crystal Pick-up.

Both available incorporating the E.S.R. STEREO £8.13.10

Pick-up, plays L.P. and 78 Records.

GARRARD MODEL TA/MKII 4-speed Player fitted high output Crystal Pick-up.

GARRARD MODEL RC/209. Autochanger 4
\$8.19.6

Speeds. High output Crystal Pick-up.

Carriage and Insurance on each above. 5/- extra.

Dept. 109 FLEET ST., LONDON E.C.4 Telephone: FLEET STREET 5812/3/4



Jtern's

For truly "Hi-Fi" Recordings

MODEL CR3/S Incorporates the COLLARO "STUDIO" TWIN TRACK 3-speed Deck, operating at 14in., 3iin, and 7iin, speeds.
H.F. Terms: Deposit £7:18.0 and 12 months of £2.17.11.

MODEL TR3/Mk.VI Incorporates the New TRUVON Mk. VI TWIN TRACK 2-speed Tape Deck operating at 3½in. and 7½in. speeds

£44.0.0

£39.10.0

There are no better value-for-money Tape Recorders on the market-if you can't call and hear them send criptive leaflet.

EACH MODEL INCORPORATES
THE MODEL HFITR3
Mk.II TAPE AMPLIFIER
(Described opposite)

Each price quoted provides for the COM-PLETE RECORDER including CRYSTAL MICROPHONE and 1,200ft. Spool of Tape.



MODEL HFG/2R The PORTABLE TAPE RECORDER

(Original Price £33.0.0)

FOR ONLY 22 gns

H.P. Dep. \$4.14.0. 12 months \$1.13.9. (Carr. and ins. 10)-carra). Incorporates The LATEST GARRARD "MAGAZINE" TAPE DECK and a High QUALITY AMPLIFIER which is entirely based on the very successful MULLARD TYPE "A" DESIGN and specifically based on the very successful MULLARD TYPE "A" DESIGN and specifically based on the very successful MULLARD TYPE "A" DESIGN and specifically based on the very successful MULLARD TOPE TO THE GARRARD TAPE MAGAZINE and 4in. SPOOL OF DUBLE PLAY TAPE. Comprises a Twin Track Recorder operating at 3in/sec, speed and providing up to 1 hour 10 mins. Playing time. Truly "Portable", weighs only \$21bs. Outstanding features are excellent performance and simplicity of operation.

THE 'ADD-A-DECK'

Incorporating
GARRAIRO "MAGAZINE"
TAPE and the MATCHED
MODEL HFIG2P
PRE-AMPLIFIER
Supplied on ONE CHASSIS (as illustrated) READY
FOR USE

ROS.

Supplied on ONE CHASSIS (as Illustrated) READY 18 Gns.
FOR USE
(Carr, & Ins. 10)- extra).
Price includes Garrard Magazine and a 4in. Spool Double Play Tape
H.P. Deposit £3.16.0, and 12 months of £1.7.8.
Provides complete tape recording facilities and designed to operate through the pick-up sockets of the standard type of RADIO RECEIVER, or an AMPLIFIER, from which really first class reproduction is obtained. It consists of a Twin Track Deck connected to the Pre-amplifier and operates at 3/in/sec. speed providing up to 1 hr. 10 mins. playing time.

FULLY DESCRIPTIVE LEAFLETS ARE PLEASE ENCLOSE S.A.E.

Stereophonic Sound by Stern's

THE "STP-1" STEREO TAPE PREAMPLIFIER DESIGNED TO OPERATE WITH

• TRUVOX MKVI TAPE DECK incorporating the latest 4-TRACK MINIFLUX TAPE HEADS.

• BRENELL MkV TAPE DECK incorporating similar 4-TRACK MINI-FLUX TAPE HEADS.

• COLLARO "STUDIO" TAPE DECK incorporating the latest 4-TRACK REUTER TAPE HEADS,

BRIEF SPECIFICATION OF PREAMPLIFIER

- PUSH PULL OSCILLATOR CIRCUIT
- 4-SPEED EQUALISATION
- FERROXCUBE OSCILLATOR TRANSFORMER
- SENSITIVE METER FOR SIGNAL LEVEL
- SEPARATE GAIN CONTROLS IN EACH CHANNEL
- MULLARD VALVES INCORPORATED



OVERALL SIZE CASE 131 x 3in. FRONT PANEL (Choice of Black or White) 14 x 34in.

PRICE

including separate Power Supply Unit. Deposit £5.4.0, 12 months £1.8.2.

£65.0.0

COMBINED PRICE SCHEDULE

THE "STP-1" PREAMPLIFIER IS OFFERED WITH TAPE DECKS AS FOLLOWS:

TRUVOX MKVI 4-TRACK MODEL...

Deposit £9.0.0, 12 months £3.6.0. £45.0.0

BRENELL MkV 4-TRACK MODEL.....

Deposit £13.0.0, 12 months £4.15.4.

• COLLARO "STUDIO" 4-TRACK MODEL..... £41.10.0 Deposit £8.6.0, 12 months £3.0.11.

STEREOPHONIC RECORD PLAYER UNITS MICROPHONES & TWIN LOUDSPEAKERS ARE AVAILABLE FROM STOCK

• THIS EQUIPMENT and the DESCRIPTIVE LEAFLET will be available late OCTOBER

PLEASE ENCLOSE S.A.E. WITH ALL ENQUIRIES

OUR MULLARD "10+10" STEREO AMPLIFIER

(described opposite) with the "STP-1" PREAMPLIFIER and one of the TAPE DECKS provide a COMPLETE STEREOPHONIC INSTALLATION.

WE OFFER
"10+10" AMPLIFIER. "STP-1" PREAMPLIFIER
and the TRUVOX MKVI DECK.
Deposit £13.0.0, 12 months £4.15.4.

£85.0.0 • As above with BRENNEL MkV DECK...... Deposit £17.0.0., 12 months £6.4.8.

 As above with COLLARO "STUDIO" DECK...... £61.10.0 Deposit £12.6.0, 12 months £4.10.2.

Please enclose S.A.E. with all enquiries.

APE EQUIPME

ADD "HI-FI" TAPE RECORDING TO YOUR EXISTING AUDIO INSTALLATION WITH

MULLARD TYPE "C" TAPE PRE-AMPLIFIER-ERASE UNIT



The "H-Fi" link to add full tape recording facilities to High Fidelity home installations. Incorporates FEROXCUBE POT CORE INDUCTOR FOR WEARITE-COLLARO-TRUVOX OR BRENELL TAPE DECKS. Includes separate power Supply Unit. P. 23.8.0 Deposit and ASSEMBLED KIT OF \$14.0.0 H.P. £3.8.0 Deposit and \$17.0.0 (Excluding power unit £11.15.0 and £14.10, respectively).

"SPECIAL COMBINED ORDER" PRICES

"SPECIAL COMBINED ORDER" PRICES
The COLLARO "Studio" Deck with the Model
"C" Preamplifier and POWER SUPPLY UNIT
ASSEMBLED AND TESTED
Deposit \$5.18.0. 12 monthly payments of \$2.3.3
As above but the TYPE "C" Unit and POWER
UNIT supplied as COMPLETE KIT OF PARTS.
Deposit \$5.6.0. 12 monthly payments of \$1.18.10
The TRUVOX MkVJ Deck (Incorporating Pause
Control and Rev. Counter) with the Model "C"
PREAMPLIFIER and POWER UNIT ASSEMBBLED AND TESTED.
Deposit \$2.0.0 and 12 months at \$2.11.4
As above but the Model "C" PREAMPLIFIER
and POWER UNIT Supplied as a COMPLETE
KIT OF PARTS
Deposit \$6.6.0. 12 monthly payments of \$2.6.2
The BRENELL MkV Deck with the Model "C"
PREAMPLIFIER and POWER UNIT ASSEMBLED and TESTED
Deposit \$3.4.0 and 12 months at \$3.7.6
As above but the Model "C" PREAMPLIFIER
and POWER UNIT Supplied as a COMPLETE KIT
OF PARTS
Deposit \$9.4.0 and 12 months at \$3.7.6
As above but the Model "C" PREAMPLIFIER
and POWER UNIT Supplied as a COMPLETE KIT
OF PARTS
Deposit \$9.4.0 and 12 months at \$3.7.6
As above but the Model "C" PREAMPLIFIER
and POWER UNIT Supplied as a COMPLETE KIT
OF PARTS
Deposit \$9.4.0 and 12 months at \$3.7.6
As above but the Model "C" PREAMPLIFIER
Deposit \$9.4.0 and 12 months at \$3.3.1

(0)

OF PARTS
Deposit #8, 12.0, 12 monthly payments of \$3.3, 1
The WEARITE MODEL 4" DECK with ASSEMBLED and TESTED Model "C" PREAMPLIFIER AND POWER UNIT incorporating
WEARITE HEADLIFT TRANSFORMER, Etc.
Deposit £11.4, 0 and 12 months at \$4.2, 1,
(Carriage and Insurance on above is 10)-extra)

£56.0.0

NEW DESIGNS!!!

MULLARD'S "10 + 10" STEREO POWER AMP-LIFIER

STERED POWER AMPLIFIER

A high fidelity design based on the famous Mullard "5-10". Provides up to 10 watts (per channel) Suberh reproduction. Frequency response flat to within 3 db from cys. 76 68 Keys at 580km.

Total Harmonic Historia and Historia and presented strictly conditions of the condition of the strictly conditions of the condition of the strictly to MULLARD's specification. Incorporates complete Mullard to the very highest technical standards and presented strictly to MULLARD's specification. Incorporates complete Mullard to the strictly to MULLARD's specification. Incorporates complete Mullard walve line-up including two of the new valves, type ECL8s, in each channel. Two specially designed GILSON OUTPUT TRANSFORMERS with 20% taps are used for ultra linear operation.

The matching CONTROL UNIT is designed to be either attached to the Amplifier (as illustrated) or can be detached for separate mounting on a Cabinet panel. Provides inputs for CRYSTAL PICK UPS. RADIO TUNING UNIT, and also for replaying from our STERO TOPE FREAMPLIFIER (CONTROL UNIT) is designed to be either attached to the Amplifier (as illustrated) or can be detached for separate mounting on a Cabinet panel. Provides inputs for CRYSTAL PICK UPS. RADIO TUNING UNIT, and also for replaying from our STERO TOPE FREAMPLIFIER (CONTROL UNIT) is designed to be either attached to the Amplifier (as MUST to the serious minded sounded entinsians. We can also supply the assembled MAIN AMPLIFIER only (excludes control unit) for operation with our DUAL CHANNEL PREAMPLIFIER, the Specifical MAIN AMPLIFIER with the ASSEMBLED MAIN AMPLIFIER with the ASSEMBLED DUAL CHANNEL PREAMPLIFIER & 300.00 beyond the swell and the supplementary of the swell and the

Dept. P.W. 109 FLEET ST. LONDOR Telephone: FLEET STREET 5817

HOME CONSTRUCTORS BUILD A HIGH FIDELITY



TAPE RECORDER LIKE THIS

for £35.0.0 Deposit £7.0.0.. 12 months at £2.11.4

FOR THIS WE SUPPLY

Complete Kit of Parts to Build the HF/TR3 Tape Amplifier. The New Collaro "Studio" Tape Deck. Portable Carrying Case (as

The New Collaro "Studio" Tape Deck.
Portable Carrying Case (as illustrated).
Rola/Celestion 10 x 6in. p.m.
ACOS Crystal Microphone and 1,200ft.
Spool E.M.I. Tape.
We will supply precisely as above—but in place of the Collaro "Studio" Deck. We will include "Studio" Deck. We will include "The Truvox Deck".
The Truvox We will include "Studio" Deck. We will include "Collaro "Studio" Deck. We will include "Collaro "Studio" Deck. We will include "Studio" Deck. We will held to the Collaro "Studio" Deck. We will the collaro "Studio" Deck. We will the deck. We OFFER—
(a) COMPLETE KIT to build the HF/TR3 Amplifier \$26.0.0
Deposit £5.10. 12 monthly payments of £1.13.2
(b) As above but with the HF/TR3 supplied AS SEMBLED and TESTED.

COMPLETE KIT to build the HF/TR3 to settler with the TRUVOX Mk. VI TAPE DECK.
Deposit £6.13.0. 12 monthly payments of £2.3.4.

(d) As above but with HF/TR3 supplied ASSEMBLED and TESTED.

£35.0.0

(e) £42.0.0

As above but with HF/TR3 supplies 13.2.

As above but with HF/TR3 supplies 13.2.

Deposit 27.0.0. 12 monthly payments of 22.11.4.

COMPLETE KIT to build the HF/TR3 AMPLIFIER with the BRENELL MK. V. TAPE DECK.

Deposit 28.2.0. 12 monthly payments of 23.1.7.

As above but with HF/TR3 supplied. ASSEMBLED and TESTED 14.7.

THE ASSEMBLED and TESTED HF/TR3 AMPLIFIES with the WEARLTS MODEL 4A DECK, incorporates Wearlte Head Lit Transformer, etc.

Incorporates Wearlte Head Lit Transformer, etc.

Carriage and Insurance on each above is 10f-extra) (D) £45.10.0

£56.0.0

MODEL HF/TR3 MK.II TAPE AMPLIFIER

Mullard Type "A" design)
A very high quality Amplifier
incorporating 3-speed treble
equalisation, by the latest
FEROXCUBE POT CORE
INDUCTOR FOR COLLAROTR U V O X - B R E N E L L
WEARITE Tape Decks,
has GILSEN Output Transformer. Includes separate
Power Supply Unit.

KIT OF £13.13.0 ASSEMBLED £17.0.0 H.P. Deposit £3.8.0 and 12 months at £1.4.11

STEREO "TWIN THREE" AMPLIFIER WITH SPECIALLY DESIGNED PORTABLE CASE

PORTABLE CASE

A most compact design
consisting of TWIN CHANNEL
AMPLIFIER based on the latest
design by MULLARD LTD. incorporating top grade Output
Transformers, and the new audio
Triode-Penrode Valves Mullard
E.C.L.86. Separate Bass and Treble
controls. Sultable for use with
Crystal Pick Ups, and capable of
genuine high quality reproduction
up to 3 Watts per channel. An
attractive and contemporary portable Case in two tone colours. The
unique leature of the design is the
foundspeaker mounthies. Two 8 x is separately baffied and mounted
in the lid, which is detachable, allowing for each speaker to
be individually positioned.
A very versatile stereo arrangement tested and guaranteed which
can be assembled in the minimum of time.
PRICE for the ASSEMBLED AMPLIFIER. Two
8 x 5 in. ROLA SPEAKERS and PORTABLE CASE
Deposit 22.16.0, 12 months of £1.0.6.

£7.15.0

£11.10

£1.1.0 £5.0.0

8 x 5in. ROLA LOUDSPEAKERS (3 ohms) each. PORTABLE CASE.....

A CHOICE OF SINGLE RECORD PLAYERS and AUTOCHANGERS is available from Stock (Send S.A.E. for details)

www.americanradiohistory.com

COMPLETE V.H.F./A.M. RADIO FOR £12.10.0

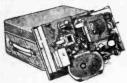


(Carr. paid)
Brand new set. In superb walnut cabinet (size 19 x 84 x 144 in. high).
Covering 80-100 Mc/s. 16-49 M., and 200-500 M. Mains trans. 200-250 v. with 2 tappings. Ferrite rod aerial for A.M. Controls: volume on/of, tone, tuning, w/change. Gram and ext. speaker position provided. Valves 12AT7, 12AH8, 6BJ6, EABC80, 6BW6 and metal rectifier. Fully guaranteed. Today's Value £20,

BUILD YOUR OWN RECORD PLAYER FOR £11.10.0

2v. amp. 57/-; B.S.R. 4-sp. autochanger 26.10.0; case 17 x 15 x 84/n. 45/-; carr. 7/6 on any two items or the lot for 211.10.0—carr. paid. Assembled in 15 mins.

TAPE RECORDER FOR ONLY £17.17.0 (10/- carr.)



NLY 217.17.0 (10/- carr.)

A QUALITY ARTICLE.
Valves EZ80, EC63, ECL82,
DM70. Acos Crystal "mike",
850ft. Tape and extra spool.
3in./sec. Mike and Radio
inputs; Vol. on/off tone,
Ext. L.S. and Monitor. Fast
forward and reverse. Cannot
be accidentally erased. Magic
Eye Indicator. 6 x 4in.
Speaker. Cabinet 14x11±x7in.
Supplied completely built
and in cabinet.

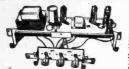


SELF-POWERED VHF TUNER CHASSIS. Covering 88-95 Mcfs. Mullard permeability Tuner, Dims. 10½ x 4½ x 51n. high. ECC85, EF91. EF91 and 2 diodes. Metal Rectifier. Mains transformer. Fully wired. and tested. Only £71.40 (carr. pd.). Room dipole 10½-300 ohm twin feeder, 6d. yd. Tuner without power pack £6.14.0 (carr. paid).



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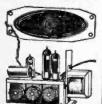
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PUSH-PULL AMPLIFIER £4.15.0

(4/- Carr.)
Brand new 200-240 A.C. mains.
Bass. trebie and vol. controls.
With valves EZ80, EC63 and
2-EL84 giving full 8 w. Chassis
12 x 3 x 3 y 3 in. With o.p. trans.
for 3-2 ohm speaker.

Front panel (normally screwed to chassis) may be removed and used as "flying panel".



3-VALVE AMPLIFIER (INC. RECT.). 4 watts. Valves ECC33 ELB4 and EZ80. Controls. volume, bass and treble. On/off switch. (Chassis size 6½ x 3 x 211n.) 64in. round or 7 x 4in. elliptical speaker. Not suitable for microphone input. A.C. only. 67. P. & P. 3/-

BEREC BATTERY RADIO IN MAKER'S CARTON.
DK96, DF96, DAF96, DL96, Two Short Wavebands 2,5 to 7 Moys and 6,5 to 17 Moys. Cabinet 12 x 71 x 6in.
ONLY 25 (2/6 p. & p.); MW and SW 25.40 (Dlus 2/6 p. & p.).

STEREO AMPLIFIER £4.15.0 (4/- p. & p.

Brand new. 200-250 A.C. Tone and volume controls each channel. EZ89; ECC83; and 2-EL84; giving 2 x 4w. Size 12 x 34 x 34 ins. O.P. Trans. for 2-30 speaker. Separate on/off switch to allow balancing to remain set.



GERMAN MADE F.M. FRONT END with ECC85 valve. Capacity tuned with reduction gear. Covers 88-98 Mcs. 42 x 3 x 31m. over valve. New. price 22/6 (2/6 post). Circuit 2/6.

"FIDELITY" 6-TRANSISTOR "CORONET" RADIO, Pocket Radio 41 x 21 x 11in. for M.W. and L.W. 12 months' guarantee. 94 gms. inc. battery, carr. paid.

CONSTRUCTORS' Bargain parcel for 20/- (3/- post) Electrolytics, tubulars, resistors, ceramics, valveholders, etc. Every parcel worth £4 at current prices.

SAVE 10/-. Swiss made Unic Shaver operating from 1.5 v. battery, usual price 58/8. Our price 50/- with battery. Takes U2 batter. Not a toy, but a shaver (carr, paid).

COLLARO STUDIO TAPE TRANSCRIPTOR. 3 MOTORS, 3 SPEED. 14, 34 and 74 I.P.S. Push buttons. £10.17.6 (10/- carr.) incl. spool.

SUPERIOR GRAMOPHONE AMPLIFIER 3 valves, 4 watt

13ł x 7łin. (2łin. front to back). 3 front controls, bass, treble, vol./ on-off. 6iln. circ. or 8 x 5in. speaker; UY85, UF86 and UL84. Mains trans. 202-240ac; "gold" fret front. ONLY 70/- (pp. 3/6).

NEW LOUDSPEAKER BARGAINS. Good Makes. 2-8 ohm. 13 x 84in. 35/- (4/-); 7 x 4in. 14/6 (2/-); 8 x 44in. 12/8 (2/-); 10 x 6in. 25/- (3/-); 5in. 12/- (2/-); 4in. tweeter 7/6 (2/-); 7 x 5in. 17/6 (2/-); 9 x 6in. 22/- (2/6). Postal charges bracketed.

MAINS OPERATED RADIO CHASSIS AND AMPLIFIER OF FAMOUS MANUFACTURE

Chassis 10 x 5\ x 4in. front to back. Valves: UBC41, UCH41, UFB4, UL84 with metal rectifier. 5in. speaker. Ferrite rod aerial. Tone, vol. and gram, position. Covers L. and M. waves. Limited quantity at only 26 (6\fo-carr.) complete with small dial. Unused and in working order.



UNREPEATABLE OFFER OF AM-FM CHASSIS AT ONLY £9.9.0 carr. pd.

A small quantity of Printed Circuit chassis by famous manufacturer. Valves UY85, UCH81, UF99, UABC90, ULB4 and UCC76, Op. trans. for 2-3 ohm speaker. Chassis 14 x 7 x 71n. Front controls concentric, left—Vol. and Tone; right—W/c and Tuning. "Gold" centre knobs provided. 2-dial bulbs. Sockets. AE: E; Ext. sp; P.U. Mains isolating provided free. Coverage Long. Med., VHF (87-101 Mc/s). Unused, slightly tarnished, but not dirty; New Mullard Valves; not our manufacture, so no guarantee.

SPECIAL OFFER OF GOODMAN 10 x 6th. SPEAKER high gauss, with doped cone specially suitable for high fidelity work. Price 2776 (post 2/6).

B.S.R. "MONARDECK" TAPE DECK SINGLE SPEED. Our price only 27.2.6 (5/6 carr.). 850 ft. first grade tape 5fin. plastic spool, 16/., post 1/.

BATTERY ELIMINATOR. For 4 Low Consumption Valves (96 range), 90 v. 15 mA, and 1.4 v. 125 mA, 42/6 (2/6 post), 200-250 v. A.C. Size 5† x 3‡ x 2in. Also for 250 mA, 1.4 v. and 90 v. 15 mA at same price.

AUTOMATIC RECORD CHANGERS. ALL 4-SPEED WITH TURN-OVER CYRSTAL CARTRIDGE (carr. 5)- extra). Latest UA14, 27,10.0. Collaro C.60 Studio model, plays any records, 7-12in. only 27,15.0. Motor board 3/6. Both UA14 and C.60 fitted mono-sural cartridge but wired (or stereo.

BRAND NEW AM/FM (V.H.F.) RADIOGRAM CHASSIS AT £14 (Carriage Paid)

Tapped input 200-225 v. and 228-250 v. A.C. ONLY.
Chassis size 15 x 6i x 5i in. high. New manufacture. 12 mths.' guarantee.
Dial 14i x 4in. in black and gold.
Pick-up. Extension Speaker. E. E., hd Dipole Sockets. Five "plano"
push buttons—OFF L.W., M.W. F.M. and Gram. Aligned and tested.
With all valves and C.P. Transformer. Tone Control Fitted.
Covers 1.000—1.900 M.: 200-500 M.: B-98 McC.
Covers 1.000—1.900 M.: 200-500 M.: B-89 McC.
Speaker and Cabinet to fit chassis (table model). 47/6 (post 3/6).
10 x 6in. ELLIPTICAL SPEAKER. 20/-, to purchasers of this chassis.
TERMS:—(Chassis) £5 down and 5 Monthly Payments of £2, or with
Cabinet and Speaker £5.10.0 down and 6 Monthly Payments of £2.
Cheap Room Dipole 10/-: Feeder 6d. yd.

This chassis is an ideal partner for the radiogram cabinet appearing on



THE "CANTATA" 6-TRANSISTOR and DIODE PORTABLE KIT



400mW push-pull output; Ferrite rod aerial; M.W. and L.W.; operates on two 4.5 v. cells; full working instructions; printed circuit, board size 8½ x 2½In. with all holes drilled; booklet of full assembly and alignment instructions; all parts sold separately. Size 9 x 3 x 7 in. Mullard transistors. Car aerial socket provided. Write for list; 8 x 2½In. speaker included tive rexine cabinet 20/- extra. Batteries 5/6 extra.

Fitted with 3 sliding doors providing room for Radio, Autochanger, 4 speakers, and record storage.



Free delivery in London area. 35/- carriage elsewhere.



TAPE RECORDER AMPLIFIER KITS



(a) For COLLARO STUDIO DECK, 11 gns. (b) For B.S.R. MONAR-DECK Twin Track, 8 gns.

These kits are complete down to the last screw and length of measured wire. Printed circuit amplifiers are tested and assembled complete with valves. Full instructions. Leaflet available. Carriage paid.

THE "CABY" TEST METERS

Prices include Test Prods, Batteries, Instruction Book. Also measure dB. Accuracy: A.C., 3 per cent. D.C., 2 per cent. A-10 £4.17.6 B-20 £6.10.0

A.10-2K ohms/v. on A.C. and D.C. velts (10, 50, 250, 600 and 1000 v.); 10K and 1M ohms; † mA. 25 mA and 250 mA. D.C. Size. 5½ x 3 ix 1½in. Weight 17 oz.

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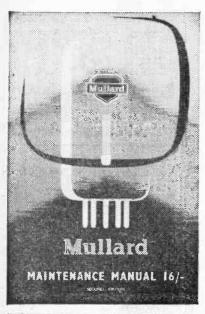
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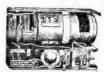


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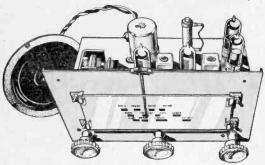
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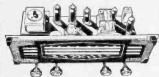
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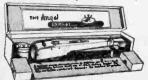
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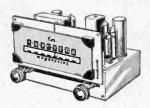
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AC/TP 33/	2 EC92	13/3	EM84		PCC89	11/6	TP25	15/-		7/6			6LD3		12J7GT		7193	
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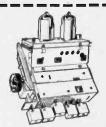
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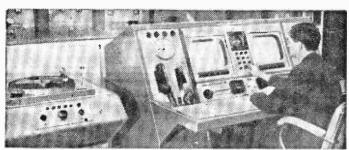
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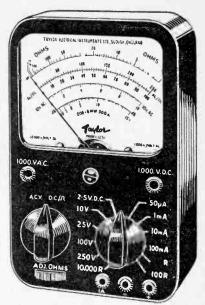
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R.S.C. (Manchester) LIVERPOOL, LEEDS, BRADFORD, MANCHESTER

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A complete set of parts to construct a good quality Stereo amplifier with an undistorted output total's watts. For A.C. mains input of 230-250 v. Outputs for matched 2-3 ohm speakers, Sensitivity 130 m.v. Ganged Vol. and Tone Controls. Preset balance control. Full instructions and point-to-point wiring diagrams supplied.

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Senior 10 wats High Fidelity output Senior 10 was and Treble "Cut" and Spost' controls of the senior senior for the senior for the senior for the senior for output senior for the senior for output senior for flass of the senior for output senior for flass of the senior for flass of the senior for flass of flass of the senior flass of flass of

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EBC33		EF50SYL		FC13		PY80		UCL83				6C6		6V6G	51_	12K8GT			8/6
EBC41		EF80		FW 4/50		PY81		UF85		354	716	6D6	5/-	6V6GT	7/9				3/6
EBF80		EF8S	71_			PY82	71_	UF89	9/_	3V4	8/-	6CH6	716	6X4	716			210DDT	
EBF89		EF86	12/6	GZ32	11/6	PY83	8/6	UL41	9/_	4DI	3/_	6F6G		6X5G	7/_	125K7		210VPT	
ECC81		EF89		HL23DI				UL84	9/_	5R4GY	916	6F6M	716	6X5GT	71_	125L7	8/-		
ECC82		EF91	5/9	HL42DI	D		10/-	UU6	19/3	5U4G	5/-	6J5GT	5/_	6/30L2	12/6	125N7G	T		
ECC83		EF91(BV				PEN25	5/_	UYIN		5V4	11/6	6J5M	616	7B6	10/6		10/-		
ECC84	10/-		716	KT2		PEN45	8/_	UY41		5Y3G		6.16	41_	7B7	8/6	15D2	7/9	×	
ECC85		EF92		KT33C		SP4		UY85		5Y3GT		617G		7C5		25A6G	8/_		
2000			_	-	_		_	1	_										_
		1 4 0 0			OHI	SPEAK	CED		_		_	-			CAR	PADIC	KIT		

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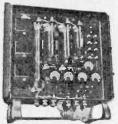
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ARP24 4/6		7'-	EZ80	6/6	QS95/10		ICSGT	7/6	6F17	7/6	9D2	3/-	350B	8/-	(091) 55%
ARP34 5/6		7/-	EZ8I	619	Q\$108/4		ID8GT	61-	6G6G	2/-	12A6	5/-	393A	15/-	VCR97 15/-
ARTH2 7/-		719		10/-	Q\$150/1		IE7GT	7/6	6H6M		12A6	7/-	705A	17/6	VCR 138 30/-
ATP4 2/9		41-	GZ32	91-	QV04/7		IG6GT	12/-	6J5 6J5G	3/6	12AT7	5/6	715B	97/6	VCRI39A
AUI 5/-		8/6	HL23	6/-	R3	8/-	ILD5	3/6		4/3	12AU6	91.	717A	8/6	35/-
AU4 5/-		7/6	HL23DD		RIO	12/6	ILN5	4/9	616	5/-	12AU7	61-	801	61-	VCRX258
AW3 4/-		7/9	HL4IDD		REL21	25/-	IR5	61-	6J7G	6/6	12AX7	7/-	803	22/6	(with scan-
AZ31 8/-		8/-		12/6	RK34	2/6	155	5/9	6K6GT	2/3	12C8	3/_	804	55/-	ning coil)45/-
BL63 6/-		9/-	KF35	5/_	RX235	10/-	IT4	4/_	6K7G 6K7GT	419	12E1	22/6	805	30/-	Photo Tubes
BS4A 5/6		7/3	KRN2A		SP2	41_	2A3	8/-	6K8G	5/9	12H6	2/-	807AME		CMG25 8/-
BT45 40/-		5/-	KT31	8/-	SP13C	4/6	2A5	8/-	6K8GT	8/3	12J5GT	3/6	807BR	5/-	931A 50%
BT83 22/6		3/6	KT32	8/-	SP41	2/6	2A6	7/-	6K8M	8/6	12K7GT		808	8/-	Special
BT9B 25/-		8/-	KT33C	4/9	SP61	2/-	2034	2/6	6L5G	6/-	12K8M	9/-	810	80/-	Valves
CY31 7/6		4/3	KT44	6/3	STV280/		2D4A	4/-	6L6	91.	125A7	716	813	67/6	2131 45/-
D41 3/3		2/6	KTW62	7/6	51.12.150	12/-	2X2	5/.	6L6G	616	125C7	4/6	815	40/-	3A/1481 45/-
D77 4/3		3/3.	KTW63		SU2150		3A4		6L34	4/6	125G7	6/6	816	30/-	723AB 45/-
DA30 12/6		61-	MH4	3/6	T41	8/-	3B7 3B24	8/-	6N7G	5/9	125H7	3/-	826	10/-	725A 30/-
DAF86 8/-		41_ 61_	MH41 ML4	41.	TH41 TP25	15/-	3E89	0	6N7GT	61-	12517	61-	829A	30/-	726A 27/6
DAF91 6/-			MS/PEN	6/-		3/.		60/-	607G	61_	125K7	4/-	832	15/-	931A 50%
DETS 15/-		5/6	NT37	0'-	TTII	16/-	(889B) 3O5GT	9/-	6R7G	61-	125L7	71.	832A	35/-	ACT6 200/-
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DK96 7/3		3/6	OD3	5/-	U27	8/-	ST4	91.	6SC7G	5/6	12SR7	61-	872A	35/-	CV691 60/-
		4/6	OZ4	5/-	U52	5/-	5U4G	5/-	6SC7GT		15D2	61.	930	8/-	KR3 45/-
DL92 6/- DL94 6/-		7/6	PCC84	7/-	UBC41	7/6	5Y3GT	6/-	65G7	5/-	I5R	5/-	954	2/-	LS7B 30/-
		7/-	PCC85	8/3	UCH42	7/6	5Z3	8/6	6SH	51.	20A2	7/6	956	2/-	V1924 22/6
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FACQI 4/6	EL 85 1	0/-	PEN2204	3/-	VP23	3/6	6AKS	5/-	6SR7	6/6	38	41.	4120	41-	£37.10
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FREQUENCY METER BC221 TECH-NICAL MANUAL 22/6. Field Telephone Type "L" Excellent

guaranteed condition, £5.5.0 per pair,

guaranteed condition, 25.5.0 per pair, carriage paid.

U.H.F. SIGNAL GENERATOR

TYPE T.S.14, 3,200-3,370 Mc/s, power measuring range 20-200 mW, P.F. output power—20 to—100 dbm below 1 mW. Power supply 115 w A.C. Price

£15. Carriage 15/-. H.T. Chokes made by Bendix Radio (U.S.A.), 3 Henry's 0.600A D.C. 25 ohms D.C. resistance 18,000 v. R.M.S. 60 cycle test, £1.12.6. P. & P. 6/-. Ditto 10 Henry's 250A D.C. 90 ohms resistance 1,500 v. R.M.S. 60 cycle test. 16/6. P. & P. 4/-. R.P. & Transpercially build for B.P.5 Transreceivers. Specially built for Parachutists during the war. Receiver superhet Transmitter crystal controlled. C.W., and phone. 2-8 Mc/s. 829 valve as output. 60 w. on C.W. 15 w. on microphone together with mains power pack

phone together with mains power pack 120/220 v. Two rotary converters to work from 12 v. battery, microphone, key and dipole aerial. Price £15. Carriage 30/-Receiver Type BC312 110 v. A.C. 1.5 18 Mc/s. £22.10.0, carriage 30/-. Receiver Type BC312. As above but 12 volt battery. £22.10.0, carriage 30/-. R109 RECEIVER. Covering 2-8 Mc/s 6 v. D.C. with set of space valves and carrier. D.C. with set of spare valves and carrier.

D.C. with set of spare valves and carrier. Brand new in original packing case. 66.18.0. including delivery in U.K. Vibrator Unit. 12 v/160 v. 35 m Amps. Exceedingly well filtered and smoothed. Excellent for car radios, Including one 6X5G valve and vibrator 17/6. P. & P. 7/-. Marconi SIGNAL GENERATOR. TF144G. 85 kc/s, 25 Mc/s. Made up to new standard. £70 delivered free. BRAND NEW ORIGINAL SPARE PARTS FOR AR88 RECEIVERS I.F. Transformers. 1st, 2nd, 3rd, 4th (for type D), 12/6 each or complete set of 6, 60/-.

I.F. Transformers. Crystal Load, 12/6

each. Plates escutcheons (for D and LF),

15/- each.

Dials (for type D), 10/- each.
Logging Dial (for D and LF), 10/- each.
Filter Chokes (for D and LF), 22/6 each. Output Transformers (for LF), 30/each.

Antenna Trimmers (LF and D), 2/6 each. Filter Condenser 3 x 4µF, £2.10.0

Condensers: 3 x .25μF (D and LF), 2/6 each. 3 x .01μF (D and LF), 2/6 each. RF Antenna Inductors (D and LF),

7/6 each. Mains Transformers (LF), £3 each.
Small Trimming Tool, 71-.
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Instruction Manual for AR88D, £1. Specially Built Power Pack for TCS

Receiver. 230 v. A.C. mains, including 6X5GT valve, £3.10.0. Carriage 5/-. 6X5GT valve £5.10.0. Carriage 3/-.
T.C.S. Receivers. Made by Collins of U.S.A. In fully guaranteed working condition. 1.5-12 Mc/s. Line up: 12SA7 (1) 12SQ7 (1), 12A6 (2), 12SK7 (3). Power requirements 12 v. L.T., 225 v. H.T. £11.10.0. Carriage 12/6.

P. C. RADIO LTD. 170 GOLDHAWK RD., W.12 Shepherds Bush 4946

R209 Reception Set. A 10-valve High-Grade Super Heterodyne Receiver with facilities for receiving R/T (A.M. or F.M.) and C.W. Frequency I-20 Mc/s. Hermetically sealed. Built on miniature Hermetically sealed. Built on miniature valves and incorporating its own vibrator power supply unit driven by a 6 v. battery (2-point connector included). The set provides for reception from rod, openwire or dipole aerial with built-in loud-speaker or phone output. Overall measurements: Length 12in., width 8in., depth 9in. Weight 23 lbs. In as new, record and supranted condition 43 10.0. tested and guaranteed condition £23.10.0, including special headphones and supply leads. Carriage £1.

Supply Unit Rectifier No. 21. Fully sealed enabling all sets built for 6 v. (R209, R109, etc.) to work from A.C. mains. Input 90-260 v. A.C. (Taps at 10 v. mains. Input 90-260 V. A. Claps at 10 V. intervals). Output excellently smoothed up to 10 amps with meter indicating exact output voltage. Measurements: 12 x 9 x 10in. Price £8. Carriage and packing 15/-.

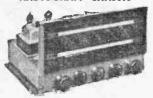
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Carbon Inset Microphone, G.P.O. Type 2/6, P. & P. 1/6. Vacuum Condenser. 32,000 v, 50pF,

Vacuum 12/6. P. & P. 3/6.
AR 88's. Completely rebuilt with new PVC wiring. Type "D" £75; Type "LF" £70.

ARMSTRONG AF208 AM/FM RADIOGRAM CHASSIS



* Fuil VHF Band (87-108 Mc/s' and Medium Band, 187-570M * 7 Valves * 5 Watts Output * 15db Negative Feedback * Separate wide range Bass and Treble Controls * 2 Compensated Pick-up Inputs * Frequency Response 30-22,000 c.p.s. ±2db * Tape Record and Playback Facilities * Continental Reception of Good Programme Value * For 3, 7; and 15 ohm speakers. Send S.A.E. for leaflet.

PRICE 22 GUINEAS Carr. Free

LATEST "E.M.I." 4 SPEED SINGLE RECORD PLAYER

Acos Hi-Fi Pick-up for LP, and/or 78, 7, 10 and 12in, records. Silent motor, heavy turntable, auto stop.

Special offer £6.5.0 post free. Stereo/Monaural £6.19.6.

BUILD THIS REPRODUCER BARGAIN

SPECIAL SINGLE PLAYER KIT

B.S.R. TU9 4-speed Gram-Pick-up Unit Handsome portable case, 131 x 15 £2.9.6 x 8fin Ready-built 3-watt, printed cir-cuit, amplifier with two valves and speaker

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I.F. TRANSFORMERS 7/6 pair

465 kc/s slug tuning miniature can ll x i x iin. High Q and good band width. Data sheet supplied.

New Boxed VALVES 90-day Guarantee

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185	7/6 6L6G	10/6 EABC		1/6
1T4	6/- 6N7M	6/6 EB91	6/- HABC	
2X2	3/6 6Q7G	8/6 EBC33	8/6	12/6
354	7/6 68A7	6/- EBC41	8/6 HVR2	4 6/6
3V4	7/8 68J7M	6/8 EBF80		9/-
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688	5/- 12A6	7/6 ECL82	10/6 PEN25	6/6
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6BH6	9/6 12AU7	8/- EF41	9/6 PL82	10/6
6BW6	9/6 12AX7	8/- EF50	5/6 PY80	7/6
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6F6	7/6 12K7	6/6 EF86	12/6 PY82	7/6
6H6	3/6 1207	6/6 EF92	5/6 8P61	3/6
6J5	5/6 35L6	9/6 EL32	5/6 UBC41	9/6
6.76	5/6 35Z4	7/6 EL41	9/6 UCH42	9/6
6J7G	8/6 80	9/6 EL84	8/6 UF41	9/6
6K6GT	6/6 807	5/6 EY51	9/6 UL41	9/6
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DK96, DF96, DAF96, DL96, 8/6 each or 30/- set.

FAMOUS MAKES ELECTROLYTICS

1/3504	2/-	TUBULAR		CAN TYPES	
2/350V	2/3	50/350V	5/6	16/45V	5/-
4/450V	2/3	100/25V	3/-	32/350V	41-
8/450V	2/3	250/25V	3/-	100/270♥	5/6
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32/450V	3/9	8+16/450V	3/9	32 + 32/450V	6/-
25/25V	1/9	8+16/500V	5/6	32 + 32 + 32/350	V71.
50/25 ∀	2/-	16+16/450V	4/3	50 + 50/350V	7/-
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TUBULA	R	32 + 32/350V	4/6		12/6

C.R.T. BOOSTER TRANSFORMERS

For Cathode Ray Tubes having heater cathode short circuit and for C.R. Tubes with falling emission. full instructions supplied.

Type A. Optional 25% and 50% Boost. 2V or 4V or 6.3V or 10.8V or 13.3V. Mains input. 12/6

TYPE A2. High quality, low capacity. 10/15pF. Optional boost 25%, 50%, 75%. Mains input.

Type B. Mains input. Low capacity. Multi output 2, 4, 6,3, 10 and 13V. Boost 25% and 50%. This transformer is suitable for all TV tubes. 21/- each.

CHASSIS MAX CUTTER

The cutter consists of three parts: a die,

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	Sizes		Prices	Key
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	sin.		 12/9	1/-
	fin.		 13/9	1/-
	žin.		 13/9 16/-	1/-
	11n.		 16/-	1/6
	1 in.		 16/-	1/6
	1¦in.		 16/-	1/6
	1%in.		 18/-	1/6
	liin.		 18/-	1/6
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	2in.		 30/-	2/3
	23/32in.		 33/6	2/3 2/3
	2∳in.		 38/6	2/3
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STANDARD, 250-0-250, 80 mA, 6.3 v. 3.8	5 a.
tapped 4 v. 4 a. Rectifier 6.3 v. 1 a. 5 v.	
	22/6
	10/6
MIDGET, 220 v. 45 mA, 6.3 v. 2 a]	15/6
SMALL, 220-0-220, 50 mA, 6.3 v. 2a 1	17/6
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HEATER TRANS. 6.3 v, 11 amp.	7/6
Ditto, tapped sec. 2. 4, 6.3 v., 14 amp.	8/6
Ditto, sec. 6.3 v. 3 amp.	10/6
GENERAL PURPOSE LOW VOLTAGE, 2a.	
	22/6
AUTO TRANS. 110-240 v. 150 w 2	22/6
Dino, 500 w 8	32/6

O.P. TRANSFORMERS. Heavy Duty 50 mA, 4/8. Multiratio, push-puil, 7/8. Ditto, 10 w., 15/8. Minitrature, 384m etc., 4/8. L.F. CHOKES 15/10 H. 60/65 mA, 5/-, 10 H. 85 mA, 10/8; 10 H., 150 mA, 14/-.

TELEVISION REPLACEMENT Line Output Transformers

from 45/- each, New Stock

and other timebase components Most makes available S.A.E. with all enquiries.

FULL WAVE BRIDGE SELENIUM RECTIFIER: 2, 6 or 12 v. 1½ amp., 8/9: 2 a., 11/3: 4 a., 17/6. CHARGER TRANSFORMERS. Tapped input 200 250 v. for charging at 2, 6 or 12 v., 1½ amps., 15/6. 2 amps., 17/6: 4 amps., 22/6. Circuit included. 4 AMP CAR BATTERY CHARGER with amp meter Leads, Fusc Case, etc., 10r 6 v. or 12 v., 69/6.

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40 Circuits for Germanium Diodes 3/-"W.W" Radio Valve Data, 6/-. High Fidelity Speaker Enclosures, 5/-Valve and TV Tube Equivalents, 9/6. TV Fault Finding, 5/-, Quality Amplifiers, 4/6. Radio Valve Guide. Books 1, 2, 3 or 4, 5/- each Transistor Superhet Receivers, 7/6.

CRYSTAL MIKE INSERT by Acos 8/8
Precision engineered.
Size only 18in. dia. x in.
ACOS CRYSTAL MIKE 40
DE LUXE STICK MIKE

LOUDSPEAKER P.M. 3 OHM. 5in. Roia, 17/6; 8in. Pleasey, 19/6. 7in. x 4in. Pleasey, 18/4; 6jin. Roia, 18/6. 10 x 6in. 27/6. 10in. Roia, 30/-4in. Tweeter, 25/-. 12in. R.A., 30/-. 14 x 8in. 45/-. STENTORIAN HF1012, 10in. 3 to 15 ohms, 10

BAKER SELHURST LOUDSPEAKERS

12in. Baker 15w. Stalwart, 3 or 15 ohma 12in. Baker ditto, foam suspension, 15 ohms .. 26 12in. Baker Ultra Twelve, 20 c.p.s. to 25 kc/s £17.10 15in, Auditorium, 35 w.,



CRYSTAL DIODE G.E.C., 2/-, GEX34, 4/-, HIGH RESISTANCE PHONES, 4,000 ohms, 15/- pr. MIKE TRANSF. 50: 1, 3/9 ea.; 100: 1, Potted, 10/6, SWITCH CLEANER. Fluid squirt spout, 4/3 tina. TWIN GANG TUNING COMDENSERS. 865 pF miniature lin. x 1½ in. x 1½ in. 10/-. 500pF Standard with trimmers, 9/-: midget, 7/6; with trimmers, 9/-. SINGLE, 50 pF, 2/6; 75 pF, 100 pF, 160 pF, 5/6. Solid dielectric 100, 300, 500 pF, 3/6.

Sond defective 100, 300, 500 p.F, 3/6.

CONDENSERS. New Stock. 0.001 m.fd. 7 kV;
T.C.C., 5/8; Ditto, 20 kV, 8/8; 0.1 m.fd., 7 kV., 9/6.
Tubular 50 v. 0.001 to 0.05 m.fd., 94, 0.1, 1/6.
0.25, 1/6; 0.5/500 v., 1/9; 0.1/350 v., 96; 0.01/2.000 v.
0.1/1.000 v., 1/9; 0.1 m.fd., 2,000 v.018. 3/6.
CERAMIC CONDS. 500 v., 0.3 p.F to 0.01 m.fd., 94,
SILVER MICA CONDENSERS. 10% 5 p.F to 500 p.F.
1/-; 600 p.F. to 3,000 p.F. 1/3. Close tolerance.
(± 1 p.F.) 1.5 p.F to 47 p.F. 1/6. Ditto 1% 50 p.F to 810 p.F. 1/9; 1.000 p.F. 1/9; 1.000

465 kc/s SIGNAL GENERATOR.
Total cost 15/-. Uses B.F.O. Unit
ZA 30038 ready made. POCKET
SIZE 24 x 44 x lin. Slight modifications
required, full instructions supplied.
Battery 7/6 extra 69V+14V. Details
S.A.E.

Wavechange Switches. 2 p. 2-way, 3 p. 2-way, short spindle 2/6; 6 p. 4-way 2 wafer. long spindle, 6/6; 2 p. 6-way, 4 p. 2-way, 4 p. 3-way, long spindle, 3/6; 3 p. 4-way, 1 p. 2-way, long spindle, 3/6;

Wavechange "MAKITS". Wafers available: 1p. 12 wafer. 2p. 6 wafer. 3p. 4 water. 4p. 3 wafer. 6p. 2 wafer. 1 wafer. 8/6: 2 wafer, 12/6: 3 wafer, 16/-: additional wafers up to 14; 3/6 each extra.

Toggie Switches, s.p., 2/-; d.p., 3/6; d.p.d.t., 4/-.

JASON FM TUNER COIL SET, 29/s. H.F. coil, aerial coil, oscillator coil, two i.f. transformers 10.7 Mc/s, detector transformer and heater choke. Circuit and component book using four 6AM6, 2/6. Complete Jason FMT/1 kit. Jason chassis with calibrated dial, components and 4 valves, 26.5.0.

Valveholders. Pax. int. oct., 4d. EA50, 6d. B12A, CRT, 1/3, Eng. and Amer. 4, 5, 6, and 7 pin, 1/-, MOULDED Mazda and int. oct., 6d.: B'G, B8A, B8G, B9A, 9d. B7G with can. 1/6, B9A with can. 1/9, Ceramic, EF50, B'G, B9A, int. oct., 1/-, B7G, B9A cans, 1/- each.

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Our written guarantee with every purchase.

S.R. Station Selhurst,

Long spindles. Midget 5 K ohms to 2 Meg. No. 8w. D.P.3w. 3/- 4/6 Linear or Log Tracks.

Volume Controls 80 CABLE COAX Semi-sir spaced in.
Stranded core. 6d. yd.
40 yds. 17/6.
60 yds. 25/-.
Fringe Quality
Air Spaced. I /- yd.

COAX PLUG ... 1/- LEAD SOCKET ... 2/PANEL SOCKETS 1/- OUTLET BOXES ... 4/6
BALANCED TWIN FEEDER yd. 6d, 80 or 300 ohms.
DITTO SCREENED per yd. 1/6. 80 ohms only.
WIRE-WOUND POTS. 3 WATT. Pre-set Min.
TV Type. All values 10 ohms to 25 K., 3/- a.
30 K., 50 K., 4/-. (Carbon 30 K., to 2 meg., 3/-.)
WIRE-WOUND 4 WATT Pots. Long Spindle.
Values, 50 ohms to 50 K., 6/6; 100 K., 7/6.

.. 2/-12.5K to 50K 10 w

AMERICAN "BRAND FIVE"

PLAS	TIC RECORDI	110	IAPE	
Double Play	7in. reel, 2.400ft	80/-	Span	re
	5in. reel, 1,200ft	37/6	Plast	tic
Long Play	7ln. reei, 1,800ft	35/-	Ree	ls
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			5in.	
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Black Crackle Paint. Air drying. 3/- tin.

HIGH GAIN TV PRE-AMPLIFIERS
BAND 1 B.B.C.
Tunable channels 1 to 5. Gain 18db.
ECC84 valve. Kit price 29/8 or 49/8
with power pack Details 6d. (PCC84
valves if preferred.)
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Aluminium Chassis, 18 s.w.g. Plain, undrilled, 4 sides, riveted corners, lattice fixing holes, 2½ in. sides, 7 x 4½ in. 4½6; 9 x 71n. 5/9; 11 x 71n. 6/9; 13 x 9in. 8/6; 14 x 11in. 10/6; 15 x 14in. 12/6; 18 x 16 x 31 x 31n. 16/6.
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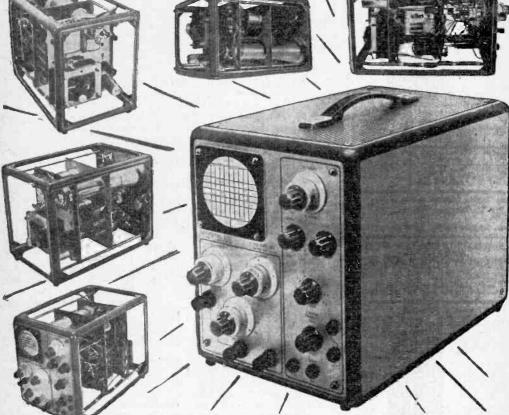
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Practical Wireless

VOL. XXXVII No. 657 NOVEMBER, 1961

Editorial and Advertisement Offices:

PRACTICAL WIRELESS

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Our Free Blueprint

S promised last month, we present free with every copy of this month's issue yet another of our new series of blueprints. As may be seen from the illustration on our cover, this amplifier is built on one of the standard 12in. group boards and it is therefore neat, compact, and very easy to build. Many readers who saw details of this form of construction for the first time in our October issue have written to say how they like this method of building apparatus, and prefer it to the customary assembly using a metal chassis. Naturally, with certain larger types of equipment, metal chassis will still have to be employed, but there are very many instances in which the group board may be used as a basis, and, apart from the ease of handling during construction, the open type of assembly greatly facilitates construction—as a matter of interest, an experienced constructor was given the parts for the "Mini-Amp" and the blueprint and the time he took to make up this amplifier was a little over

Next month, there will be another of these free gift blueprints, which will deal with a superhet receiver, and the amplifier described in this issue will constitute the output stages. This superhet will be constructed in two units on two 18-way group boards of the same type as those used for the "Tutor" and the "Mini-Amp". One group board will form the frequencychanger stage (using one transistor) and the other the I.F. amplifier (using two transistors). The two units (together with the "Mini-Amp") will form a sensitive, 7-transistor superhet, with its own internal aerial, equal in performance to many commercial designs. Order your copy of the December issue

now; the demand will be great.

Multimeter Blueprint

With every copy of the October issue of our companion journal Practical Television is a free gift blueprint for a comprehensive multimeter—the latest Practical Television design. This blueprint is the result of several months' work, and, although this design has been described in Practical Television it should not be thought that it is only suitable for the television enthusiast; in fact, the multimeter is equal in performance to many commercial instruments and will be found worthwhile on any experimenter's work bench, whether his main interest lies in television, radio, or electronics.

A Film Show

NOTHER film show has been arranged in collaboration with A Mullard Ltd. It will be held at Caxton Hall, Westminster, and readers are invited to send for their free tickets which are now available from these offices. The films will be shown on Friday, February 2nd, 1962, and the programme will begin at 7.30 p.m. When applying for tickets, enclose a stamped addressed envelope (at least 31 in. x 6in.). Mark your envelope "Caxton Hall" in the top left-hand corner.

Our next issue, dated December, will be published on November 7th,

Round the World of Wireless

POTENTIAL AND CURRENT NEWS

Broadcast Receiving Licences

THE following statement shows the approximate number of Broadcast Receiving Licences in force at the end of July, 1961, in respect of wireless receiving stations situated within the various Postal Regions of England, Wales, Scotland and Northern Ireland. The numbers include Licences issued to blind persons without payment.

Region				Total
London				687,209
Home Counties				647,133
Midland	4.00			471,468
North Eastern				507,129
North Western				437.197
South Western				385,019
Wales and Border	Counti	es		224,110
Total England and	Wales			3,359,265
Scotland				374.562
Northern Ireland				116.560
STORESTON IN CHARGE	••	• •	-	110,000
Grand Total				3.850.387

Record Radio Show

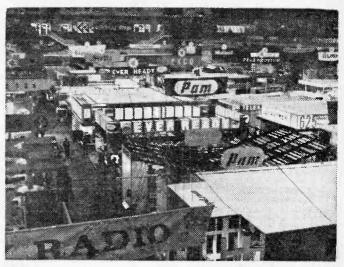
THE 1961 Radio Show, which ended on September 2nd, had attendances averaging nearly 40,000 a day; the highest since it moved to Earls Court from Olympia in 1951. Most manufacturers were well pleased with the amount of business transacted, and several claim it to be the best show for five years.

The next Radio Show will be held at Earls Court, London, from August 22nd to September 1st, 1962.

Radio Bournemouth

DURING September, the BBC held an exercise in local broadcasting, when Radio Bournemouth went "on the air". This exercise was spread over seven days—September 5th to 11th inclusive.

Each day there were four or five hours of local programmes. The many aspects of local interest which, were covered, were given as bulletins, talks, interviews and discussions. Among others, items on local government, sport, voluntary organisations and well-known local personalities were of particular interest to the people of Bournemouth, Poole, and Christchurch.



A general view of this year's Radio Show, at Earls Court, London.

Although the station was in operation continuously throughout each day from 6.30 a.m. until late evening, not every minute of the day was filled with local material. In between local items, the station manager linked his station with one of the BBC's networks. to draw programmes from the Light Programme or Home Service.

New Communication System

A NEW communication system has been installed in the 24 bungalows and the flat of the resident warden on the Church View Estate, Eastwood, Nottinghamshire. Each has been equipped with a Portaphone—a unit which when plugged into an electric mains socket forms a communications system with any other similar unit plugged into the lame circuit.

The Portaphone is made by Labgear Ltd., a member of the Pye Group, and its use in this system will ensure that the occupants of Church View Estate — mostly elderly people living alone—are able to contact the warden immediately in any emergency.

The system operates free of any interconnecting cables as the speech travels along the electricity mains wiring.

Iraqi Contract

A CONTRACT to the value of approximately £100,000 has been signed by the Iraqi Port Authority and Pye-Telecommunications Limited of Cambridge for the supply and installation of several VHF and UHF radiotelephone networks.

VHF telephone services are to be installed at Margil for Basrah airport: the Ports' ambulance, fire-fighting units, electricity distribution department and the maritime services. Four other VHF communication systems are to be supplied for the maritime services at Al-Wasillah, Fao, the Deep Water Berth and Um Qasir. A UHF telephone link between Fao and the Deep Water Berth and a VHF telephone service aboard the Ports' maritime vessels is also included in the contract.

It is anticipated that the entire scheme will be fully operational early in 1962.

German Radio and TV Show

BETWEEN August 25th and September 3rd this year the German Radio, Television and Phono Exhibition was held in Berlin.

One hundred and fifty-eight exhibitors had on show equip-

ment appertaining to all branches of the radio, television and record industry.

Telephone Exchange for Infirmary

A NEW telephone exchange for the Radcliffe Infirmary, Oxford, one of Britain's leading teaching hospitals, is to be supplied by Associated Electrical industries Ltd. It is to be installed by early 1962 by the Private Telephone Department of AEI Telecommunications Division.

As a result of the installation of this up-to-date exchange, a considerable economy in the number of telephone instruments needed will be achieved.

The exchange will cater for 550 telephones in the Infirmary, and their users will be able to call each other by dialling, and call outside telephone subscribers through the local GPO exchange from which there will be 35 public exchange lines. Oxford now has Subscriber Trunk Dialling and direct dialling of trunk calls will be possible from certain extensions.

Three operators will staff a manual switchboard suite to handle incoming calls and provide service where a personal agency is necessary. The switchboard will be of the new AEI cordless type where, instead of the familiar plugs and cords, keyswitches are used to set up the call; and where the normal dial is superseded by press buttons which operate an automatic dialling unit known as a keysender.

New Export Company

A NEW subsidiary company of E. K. Cole Ltd., has recently been formed—Ekco Export Ltd. The new company will handle the export of radio, television and car radio receivers, electric heating and plastics products produced by the Ekco Group and will be responsible for maintaining and expanding overseas manufacturing arrangements.

manufacturing arrangements.
Mr. T. C. Cleveland, formerly
Export Manager of E. K. Cole
Ltd. is Director and General
Manager of Ekco Export Ltd.
Other directors are: Mr. W. M.
York (chairman), Mr. J. Corbishley and Mr. D. J. Cole.

The new company will operate from the main Ekco works at

Southend-on-Sea and a Personal Exports Department and show-room for radio and television receivers will be opened in London at 41-47 Old Street, E.C.I.

New Factory in Crawley

THE commercial divisions and most of the productions staff of Mullard Equipment Ltd. moved to their new factory at Crawley New Town, Sussex, on September 4th.

About 600 staff moved to the new plant. In addition, staff recruitment has been going on at Crawley for some time, and it is hoped that up to 200 will be engaged by the end of this year.

The new 134,000sq.ft plant is on a site of 17 acres on which expansions are planned to be made in the future. The new buildings are constructed so that they can conveniently form part of a larger unit.

Research Scholarships

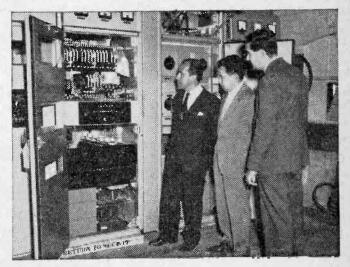
EACH year the BBC awards research scholarships (valued at £500 per annum) to university graduates in electrical engineering or physics, giving them the opportunity to work for a higher degree at any university in the

United Kingdom, not necessarily the one from which they graduated. The scholarships are normally for two years in the first instance, with the possibility of extension in suitable cases where this is required. The scholarships are limited to male subjects of the United Kingdom, and the only condition applying to the subject for research is that it must be in those fields of telecommunications or physics which have an application to sound or television broadcasting.

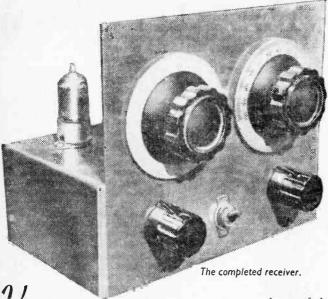
This year three scholarships have been awarded—one for one year and two for two years. The scholarship for one year has been awarded to Mr. J. Elliott who graduated at Imperial College, University of London, with first-class honours in electrical enginering in 1957.

One scholarship for two years has been awarded to Mr. K. L. Hughes who graduated from Birmingham University with first-class honours in electrical engineering.

The second two-year scholarship has been awarded to Mr. B. J. Tilley who has graduated with second-class honours in electrical engineering from University College of Swansea.



Spending a few days at Marconi's, Chelmsford, recently, in discussion with Communications Division, were two senior engineers from Empresa Nacional de Telecomunicaciones, Bogota, Colombia—Senor Dn. I. Ancines (left) and Senor Dn. J. A. Velex (centre). They are pictured here inspecting a IOkW H.F. ISB Transmitter type HS 71 in the test department at the company's Chelmsford works with B. W. Bardwell of Communications Division.



ERY long range reception is possible with a short wave 1-valver, and the addition of an amplifying stage provides a useful increase in volume. The circuit described here uses two 1T4 valves, but any equivalents, such as the CV785, W17, or DF91 are equally suitable. The two wavebands permit tuning from approximately 10m to 60m, and thus cover the most popular S.W. bands.

Bandspread Tuning

Bandspread tuning is fitted, and allows accurate logging of transmissions. This method of tuning does not make construction difficult, as no reduction drives are needed. The circuit is shown in Fig. 1, and 150pF condenser the adjusted to the required band, which is then covered by means of the 15pF condenser, The small capacity of the latter makes tuning easy, and dial readings can be noted down so that they can be returned to when necessary. Two coils are fitted, the required coil being selected by means of the 2-way switch.

For high tension, 45V or more will be needed. A 45V supply can if necessary be obtained by wiring two 22½V batteries in series. Less than 45V is not recommended, as insufficient reaction is available. A standard 67½V battery may also be used, and would do very well.

The valve filaments require 1.4V and this can be obtained

THE P.W.

A SENSITIVE SHORT-WAVE RECEIVER COVERING IOM TO 60m IN TWO RANGES

from a 1½V battery, as used in portables. Alternatively, dry cells such as found in torch and lamp batteries may be used, provided they are wired in parallel. With such batteries, the zinc case is negative. Cells must not be wired in series, nor must more than 1½V be used. The filament consumption is only 0·1A.

Components

There is reasonable latitude in the selection of components, so items to hand may possibly be used. For bandspreading, a condenser of about 10pF to 20pF is satisfactory. Some

denser of about 10pF to 20pF is satisfactory. Some S.W. condensers can easily have plates removed, to reduce the capacity. For bandsetting, 100pF or 200pF could be fitted, if to hand, with some modification in the band coverage.

The H.F. choke must be capable of working over the frequencies tuned, so a reliable S.W. or all-wave component is needed. As the insulation of the $0.01 \mu F$ coupling condenser must be very good,

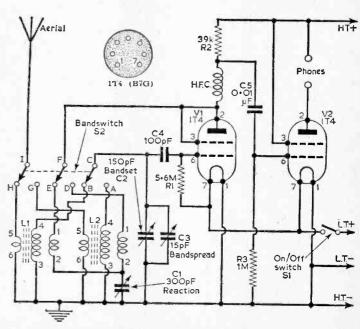


Fig. 1.—The circuit diagram of the receiver.

Beginners' S.W. Two

By F. G. Rayer

a mica condenser, preferably new, is best here. Leakage would cause a positive voltage to reach the amplifier valve grid.

It is worth noting that the receiver can be constructed as a 1-valver, merely by omitting the 39k resistor, 0.01 µF condenser, 1M resistor, and second 1T4 valve. Phones are then connected from the H.F. choke to H.T. positive. Quite good results may be obtained with the single valve.

Chassis Preparation

Chassis and panel should be drilled before mounting any parts. A chassis about 7in. x 4in. x 2in. deep will be convenient, but some change in

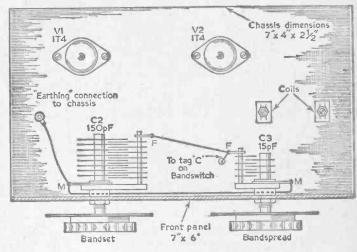


Fig. 2.—The above-chassis wiring of the set.

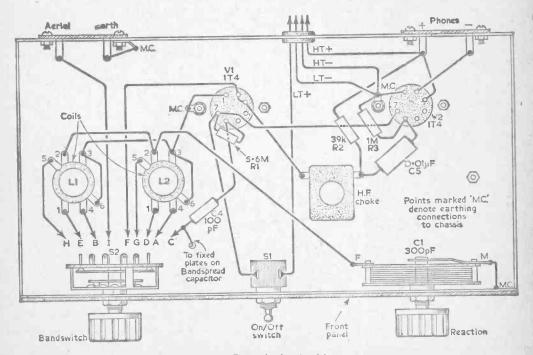


Fig. 3.—The underchassis wiring.

size will not affect performance. The panel can be about 7in. x 6in.

Fig. 2 shows the top of the chassis. Holes for the B7G holders can most readily be made with a chassis cutter or valveholder punch. If these are not available, a ring of small holes may be drilled, the piece broken away, and the hole smoothed with a round or half round file.

Holes for the 150pF and 15pF variable condensers should also be drilled. The three holes near the bottom of the panel are then marked and drilled. The panel is then positioned against the front runner of the chassis, and the location of the holes is marked. The chassis is then drilled, so that the two switches and reaction condenser will

hold the panel and chassis together.

At the rear of the chassis, drill or punch clearance holes for the two socket strips. Ensure that aerial and phone sockets will be well clear of the

metal. Holes are also made to take the coils, but these are best left off until later.

Wiring

Fig. 3 shows the wiring and component layout under the chassis. The three points marked "M.C." consist of tags bolted to the chassis, so that leads may be soldered to them. Place the valveholders so that the sockets come approximately as in Fig. 3.

Soldering will cause no difficulty if the iron is really hot, and tags and leads are perfectly clean. Use a cored solder, as sold for radio work. Do not carry solder to the joint on the iron. Instead, apply iron and solder to the joint, so that the flux

can take effect where required.

The moving plates tags of both 150pF and 15pF condensers are wired together, as in Fig. 2, and the lead soldered to a soldering tag which is bolted to the top of the chassis. The fixed plates of these variable condensers are similarly joined, and a lead goes through the chassis to the 100pF fixed condenser, and switch (tag C in the switch diagram).

Use flex for battery connections, and fit suitable plugs, or identify the leads so that the filament circuit will not be taken to the H.T. battery in

Most of the wiring in Fig. 3 can be done first, the coils being left until last. All leads in the coil,

COMPONENTS LIST

Two IT4 valves
Two BTG valveholders
Fixed condensers: 100pF and 0·01 µF (mica)
Resistors: 39k, 1M, 5·6M
3-pole, 2-way switch
300pF reaction condenser
SWQ1 and SWQ2 coils (Osmor)
H.F. choke (Osmor)
150pF and 15pF or similar short wave tuning condensers
Two 2\frac{3}{4}in. diameter or similar dials and knobs
Two 1 in. knobs
On/off switch
Two double socket strips
Chassis approximately 7in. x 4in. x 2\frac{1}{2}in. deep
Aluminium panel approximately 7in x 6in.

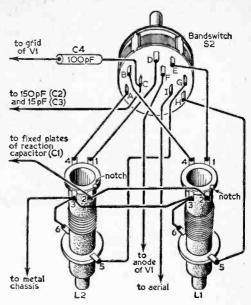


Fig. 4.—The wiring of the coils and the switch SI.

switch, and tuned circuit section should be reasonably short and direct. With the reaction condenser, the moving plates tag goes to chassis, and the fixed plates tag to tags 2 of the coils.

Coil Connections

When the receiver is viewed from underneath and behind, the coil and switch connections will appear as in Fig. 4. Note that each coil has a notch, for tag identification.

Wire tags 6 to tags 3 before mounting the coils, and also solder leads a few inches long to tags 5. The higher wavelength coil (which has most turns) is placed at the right, in Fig. 4. The coils can then be inserted, and secured with their clips. Ensure that tags 5 and 6 cannot touch the chassis.

The remainder of the wiring, as shown in Fig. 4, can then be completed. Connections should be short and direct, but clear of each other. The same identification letters are used in Figs. 1, 3 and 4, and no difficulty is likely to arise in wiring up the switch correctly.

Dials and Knobs

Fairly large knobs are best for 150pF and 15pF condensers, but they need not necessarily be of the type illustrated. Scales (0-100 or 0-180) should be fitted to knobs or panel, so that readings can be noted.

For reaction, a very small knob makes operation a little difficult, as the reaction setting is critical, with weak signals. The band selection switch can be of the same type, to match.

Phones should be of the usual medium or high impedance type, and low impedance surplus phones are likely to be unsatisfactory.

If an earth is available, it is taken to a plug which is inserted in the socket marked in Fig. 3. An earth lead may be connected to an

earth spike, or water pipe, or any similar metal object in contact with the ground. The lead should not be connected to gas pipes, hot water pipes, or mains earth circuits.

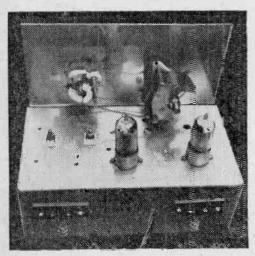
For general purposes the aerial can be a single uncut length of insulated wire, forming both aerial and lead-in. The actual length which can be erected will depend on circumstances, and may be anything from about 20ft to 45ft or so. The wire and downlead should be as far from walls and other earthed objects as possible. One or two aerial insulators are used at each suspension point. Reception of distant stations is, of course, possible with an indoor aerial, but volume will be reduced. It is thus worthwhile trying to fit up a reasonably effective aerial.

If a really long aerial is available, it can be used. If it is found that reaction is difficult to obtain on some frequencies, a small fixed or pre-set condenser should be included in series with the lead-in, at the aerial socket. A capacity of about 50pF is generally satisfactory. If a pre-set is used, adjust it for best

results.

Using the Receiver

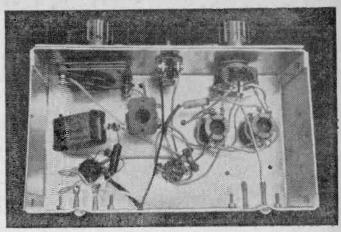
If the constructor is not familiar with S.W. reception, it should be remembered that the results obtained on the various bands depend on the time



Rear view of the set.

of day, and other conditions. Most broadcast stations use wavelengths near each other, and are thus found congregated into bands, such as the 49, 41, 31, 25 and 19m bands. Morse and various other transmissions will be heard between these bands.

The actual tuning range of each coil, and also



The underchassis wiring.

reaction, will be modified to some extent by the core position. The cores should be adjusted until reaction is easily obtained. If necessary, some modification of this position is possible, to change band coverage. The cores should then be locked with nuts, as moving them will change dial

readings.

The reaction condenser should be closed slowly until a sudden increase in sensitivity, and oscillation on tuning through a station, shows that the optimum position has been passed. While tuning, the reaction control is adjusted to keep the receiver just below the oscillation point. In this condition it is extremely sensitive. If the reaction control is insufficiently advanced, only powerful stations will be heard. On the other hand, if the control is turned too far, results will be very poor. However, the way in which the reaction control operates will soon become apparent.

For reception of ordinary stations, or telephony (voice and music) the receiver is kept just below the oscillating point, as described. The setting is not critical with powerful stations, but is quite exact with weak stations. To receive C.W. Morse (unmodulated carrier) the reaction control has to be

advanced to the oscillation point.

The 150pF condenser is only used to locate the various bands. The dial reading of this condenser should then be noted down as accurately as possible. Tuning is then carried out on the 15pF condenser, in conjuction with reaction, as described.

If there is any variation in the efficiency of the 1T4 valves, the best valve should be placed in the

detector position.

It is not very likely that any fault should arise in the receiver, but if no results are obtained, a few simple tests should localise the trouble. First, the phones may be connected across the 39k resistor. If normal 1-valve reception is then obtained, the amplifier stage is faulty. The valve can be tested by placing it in the detector position.

If results are absent with the 1-valve circuit, check the detector stage wiring. If reception is obtained with one coil, but not the other, suspect the switch connections, or the wiring to the inoperative coil.

A Simple Condenser Bridge

AN INEXPENSIVE INSTRUMENT WITH THREE RANGES

By G. A. W. Partridge

T is obvious that the efficiency of electronic equipment depends largely upon the components. Resistors are quickly checked with an ohmmeter, but unfortunately condensers are far too often taken for granted. These are the very components that can mar the efficiency of a circuit. Old condensers should be tested before they are used again, and it is an idea to check up on new ones as well.

Range

This simple capacity tester can be made up in a few hours. It is easy to use and costs only a few shillings. There are three ranges: 100pF-1000pF; $1000pF-0.01\mu F$; $0.01\mu F-0.1\mu F$. which are adequate for most purposes. However, provision has been made for an extra range if necessary. The circuit is shown in Fig. 1.

The various components are mounted in a box (Fig. 3). The dimensions and constructional details are clearly seen in Fig. 2. The condensers used as standards must be of a high grade as the accuracy of the instrument is largely dependent upon them. The variable resistance is a 1M

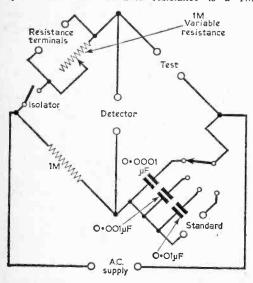


Fig. 1.—The circuit of the bridge.

volume control potentiometer. Both resistors must be non-inductive. An old radio wave change switch will be suitable as a range switch. Tests are carried out in the following manner:—

The A.C. supply is drawn from an audio frequency oscillator which is set to give a good clear note of about 1000c/s; a pair of headphones or an amplifier and loudspeaker is connected to the detector terminals; the condenser under test is then connected to the test terminals. A suitable range is selected and the isolating switch turned on. The variable resistance is then turned until the A.F. note is no longer heard or is at its minimum value. Great care must be taken in finding the "null point".

The isolating switch is now turned off, and the resistance in circuit of the variable resistance measured by connecting an ohmmeter to the terminals marked Resistance.

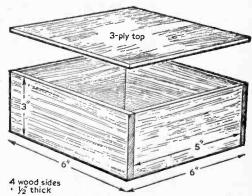
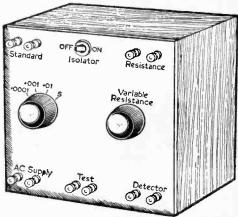


Fig. 2 (above).—The construction of a suitable case for the unit.

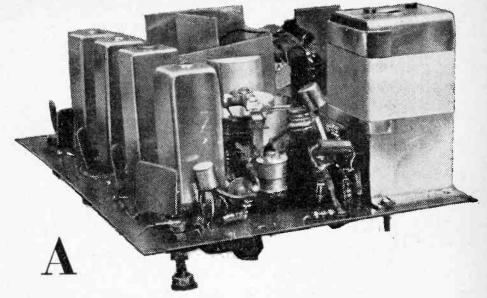
Fig. 3 (below).—The completed unit showing the various positions of components on the front panel.



From the formula: $C = Range \times 1,000,000$

Circuit variable resistance, the capacity of the condenser is determined in microfarads.

(Continued on page 607)



Transistorised VHF Superhet

THE "PRINTED" CIRCUIT AND HOW TO MAKE IT

By D. R. Bowman

(Continued from page 494 of the October issue)

HE receiver is based on a piece of laminated copperclad plastic measuring approximately 10½in. x 6in. The copper layer serves not only as a source of conductors but also as a metal chassis. The prototype receiver was constructed on a sheet of very ordinary laminated board, but for reliability and good electrical properties the board specified is "Bakelite" grade DH74. This grade is an epoxy glass fibre laminate and is rather expensive; if cost is a major item, "Bakelite" grade E60 will be found very efficient, and the cost is about a quarter that of the DH74. It is important that the sheet is mechanically stable—the thickness of the board should be not less than ½ioin.

The first step is to mark out the position of the components, beginning with the large items such as transformers, heat sinks, tuning capacitor and volume control, and following with the I.F. transformers which are contained in four cans. Marking out can be done with a ball-pen, very soft pencil or fine brush and white watercolour or

drawing ink. Figs. 9 and 11 show the layout suggested, which includes the necessary conductors marked out. Conductors are shown white, while conducting tags, surrounded by an insulating space,

are marked by a full spot surrounded by a ring. These latter are used for anchoring component wires which need to be insulated from the copperclad board.

Layout

The I.F. transformers separate the I.F. transistors, and the R.F. and frequency changer stages are mounted to the right of the tuning capacitor; there is plenty of room in the layout given. The audio stages begin

Bakelite former

Bakelite panel

Copper coating

6BA nuts and washers

Fig. 8.—The method of spacing the I.F. coils from the chassis—see also Fig. 5, on page 494 of the October issue.

directly below the ratio detector, and continue across the bottom part of the board.

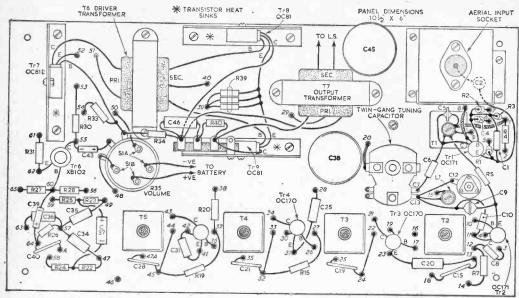


Fig. 9.—The above-chassis layout and wiring of the receiver.

The marking out of all components, down to the last resistor and capacitor, must be carried out before etching is put in hand. When, by comparison between the marked laminate and the

theoretical diagram, it is quite certain that full provision has been made, the preparation of the board can begin. First it must be kept in mind that as little copper as possible is removed, and

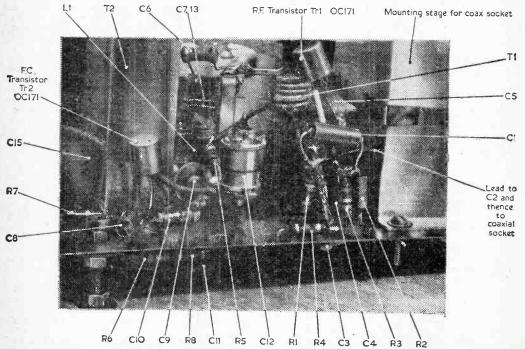
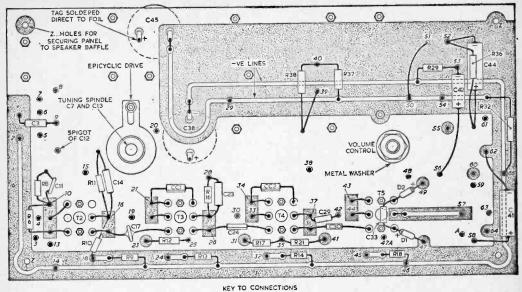


Fig. 10.—The layout of the R.F. stage of the receiver—this constitutes the only critical part of the set.



CONNECTIONS THROUGH PANEL
CONNECTIONS DIRECT TO FOIL

CONNECTIONS SHOWN ARE ANCHORING POINTS FORMED BY ETCHING AWAY A RING OF COPPER CONNECTIONS TO I.F. TRANSFORMERS

Fig. 11.—The below-chassis wiring—this diagram should also be used to mark out the printed wiring before etching; the copper which remains after etching is shown unshaded.

that the "earth" part of the copper is electrically continuous. Sufficient space must of course be left for insulation where needed; the width of conductors should be not less than $\frac{1}{8}$ in. and the anchor tags should be of $\frac{3}{16}$ in. diameter, surrounded by an $\frac{1}{8}$ in. width of insulation where the copper is etched away.

"Resist" Solution

A "resist" material is now made up by dissolving for of shellac in about 40z of methylated spirit. This will take some while to dissolve, and is conveniently left overnight to complete the process. If some sealing-wax is added at the same time, or a little mahogany spirit dye, the resist solution will be found more visible when applied.

A water-colour brush is used to apply the solution which should be reasonably "thick" or else

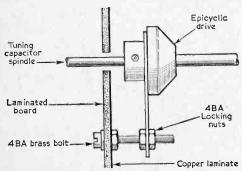


Fig. 12—The mounting of the epicyclic drive for the tuning capacitor.

it may run where not desired. A steady hand is needed, and some practice is essential; this may well be carried out on a sheet of glass or paxolin. All parts which are to be conducting must be covered, not only the "conductors" but the "chassis" part of the board as well—shown unshaded in Fig. 11. The only parts not covered are those which are to be etched away.

Mistakes can be corrected by a plug of cotton wool damped (not saturated) with methylated spirit; the plug should be turned frequently so that all traces of the resist are removed from the area concerned. Thorough cleaning is essential and is not easy, so mistakes are best avoided. When it is decided that all is in order, the resist coating is gone over again to thicken it. Finally, the prepared board is left overnight to dry.

Etching Solution

A solution of ferric chloride, FeCl₃, is made up by dissolving 40z ferric chloride in 60z water, adding 10z concentrated hydrochloric acid—HCl. (Commercial "spirit of salts" is suitable.) This will form a very deep orange clear solution which is corrosive and must be kept in a well-corked, labelled bottle well out of the way of food and out of the reach of children. For use, the solution is poured into a flat container such as a photographic dish, and the laminated board immersed in it.

Etching will take a little while to accomplish; about an hour should be allowed but it may take longer, depending on the temperature. When the copper is completely removed, where required, the board should be removed from the solution, washed for a few minutes in running water, and

dried with a soft cloth.

The removal of the resist is best effected by soaking the board in methylated spirit for 10-15 minutes, and then rubbing briskly with a plug of cotton wool damped with methylated spirit. Finally, hot water is used with some kitchen seouring powder on a rag; this will give a bright surface ready for silver-plating if it is now desired to carry out the process. If an electrolytic method is used, only the "chassis" can be plated, but this is relatively quite effective.

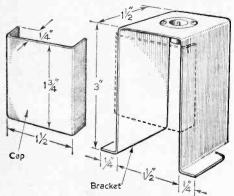


Fig. 13.—The mounting bracket for the coaxial socket in the R.F. stage.

All necessary holes should now be pierced. For holes which carry one wire, a $\frac{1}{32}$ in. drill is enough, but where several wires will be anchored at one point, a hole of 16 in. diameter will be needed. It is not strictly necessary to drill at all points where "earth" connections have to be made; if a connection is carried through the board a hole will of course be needed.

All the components are now mounted in position, and this is best done direct from the theoretical diagram following the logical layout. When fixing the I.F. transistors, all wires but the wire are covered with thin insulating The wires are not cut down at all, and sleeving. this will be found not only convenient for mounting but safe for soldering. Nevertheless a really hot iron should be used, to minimise the time of the soldering operation.

R.F. Stage Layout

In the R.F. stage, it is most important to avoid capacitive coupling between collector and emitter. For this reason, the R.F. stage is a three-dimensional assembly and layout is somewhat critical. Fig. 10 which shows the arrangement of components should be used as a guide.

The coaxial socket for the aerial is carried on a bracket of bent-up aluminium sheet. Dimensions

are given in Fig. 13.

The "cap" is clipped over the vertical sides of the stage to shield the aerial connection from the rest of the R.F. assembly, as shown in Fig. 14 and the illustration of the R.F. stage.

The bakelite formers for R.F. and F.C. stages may readily be affixed to the laminated board with the impact adhesive used according to the manufacturers' instructions and remembering that once

contact has been made very little further drying can take place. It is therefore essential to ensure that complete drying has taken place before putting the former in contact with the laminated board. After preparing the surface, at least ten minutes should be allowed for drying in a room at 68°F.

The Tuning Capacitor

The specified capacitor is mounted, by two screws, at right angles to the printed circuit board, and is operated by means of an epicyclic drive. The lug of the epicyclic is clamped to the board by means of a 4B.A. brass bolt passed through the board (see Fig. 12).

In the prototype receiver, a circle of Perspex was cut, and a hole drilled in the centre to make a good force fit over a standard knob, to fashion a tuning knob of attractive appearance. A pointer fixed to the epicyclic was arranged to move in front of a scale cut out of paper and stuck to the front of the cabinet.

Mounting of the Loudspeaker

If the loudspeaker is mounted on the same panel of the cabinet as the printed circuit, microphony may be experienced at moderate volume levels. To minimise this difficulty, the speaker may be mounted on an ellipse of rubber surrounding the hole in the cabinet. Adhesion between speaker and rubber, and rubber and cabinet, can be secured by one of the contact adhesives.

A cut-out will be needed in one of the folds used for fixing the mounting bracket to clear a bolt used for mounting the printed circuit to the loudspeaker baffle (see Fig. 9).

Alignment

Alignment is carried out as follows, and signal generator capable of covering the frequen-

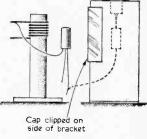


Fig. 14.—The position of C2 inside the mounting bracket.

cies of 10.7Mc/s and about 100Mc/s is required. (Amplitude modulation will be needed.)

1-Set the generator to 10.7Mc/s and switch on. Allow ten minutes for warming up. Switch on

the internal modulation (A.M.)
2—Switch to "high" output and bring an insulated wire from the signal generator close to the base wire of Tr5. Rotate the core of T5 (collector winding) for maximum sound in the loudspeaker. Align the slug of Tr5 base winding in T4 for maximum output.

3—Transfer the wire from the signal generator to near the base wire of Tr 4. Align cores of T4 for maximum output. Align the slug of Tr4 base winding in T3 for maximum output.

The alignment of the I.F. stages is now almost complete; next month the alignment of the discriminator and oscillator circuits will complete the receiver.

(To be continued)

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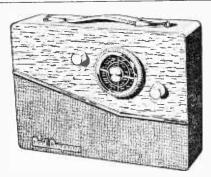


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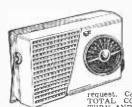
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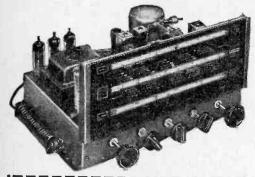
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Electrolytic

SOME OF THE USES AND FAULTS OF THESE COMPONENTS

Capacitors

By G. J. King

HE primary applications of electrolytic capacitors as reservoir and smoothing components in H.T. filter circuits are probably amongst the most well known. When a radio produces a loud hum from the speaker which is unaffected by the setting of the volume control, one can be reasonably sure that the reservoir or smoothing electrolytic condenser is open-circuit or low in value.

Short Circuit

When the set is dead, and the rectifier starts sparking accompanied by overheating of the surge limiter resistor, again, the reservoir condenser should be suspected, but this time for a short-circuit. If the smoothing or filter resistor also heats up badly, a short-ciruit in the smoothing electrolytic is most likely responsible. These components, anyway, should be the first to be checked.

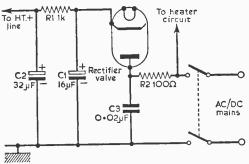


Fig. 1.—The H.T. circuit of a receiver; C1 is the reservoir capacitor and C2 the smoothing capacitor.

In Fig. 1 is shown the H.T. circuit of a typical receiver. The electrolytic capacitors are C1 and C2, from which it will be seen that the symbol for electrolytics differs slightly from the ordinary capacitor symbol, such as C3. Electrolytic capacitors are polarised. That is to say one terminal is marked positive (usually with a blob of red paint), while the negative terminal is sometimes the metal can in which the capacitor is housed. The positive side is signified by the narrow, open rectangle of the symbol.

The reservoir capacitor is the one connected between the output of the rectifier and negative H.T. or chassis (C1), while the smoothing capacitor is the one connected between the H.T. line side of the filter resistor or choke and chassis (C2). The filter resistor in Fig. 1 is R1: R2 is the surge limiter and C3 is a mains filter capacitor.

Voltage

Electrolytic capacitors are given two voltage ratings: the maximum working voltage and the maximum surge voltage. The working voltage is the direct voltage applied to the capacitor (as would be measured on a D.C. voltmeter) together with the peak ripple voltage. The ripple voltage is governed by the type of rectifier circuit used and by the H.T. current.

The surge voltage is the voltage which develops across the capacitor before the equipment starts taking current, or the voltage across the capacitor when the H.T. line is open-circuited.

Ripple Current

The ripple current is another very important factor in the rating of a capacitor and one which is not always fully appreciated by the experimenter. An H.T. reservoir capacitor, for example, is required to pass a considerable alternating current

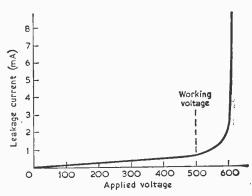


Fig. 2.—This graph shows how the leakage current increases rapidly when the working voltage is exceeded.

by the very nature of its application. This A.C. is termed ripple current, and it is essential that this does not exceed the ripple current rating of the capacitor.

Ripple current is directly related to such factors as the amount of D.C. drawn by the set, the source impedance of the H.T. circuits, the value of the capacitors, etc., and is rather difficult to assess directly in these terms. However, a fairly reasonable idea of the ripple current can be obtained by multiplying the total direct current drawn by the set by 1.5 for full-wave rectifier circuits and by 3 for half-wave rectifier circuits.

Thus, if the half-wave circuit in Fig. 1 were supplying, say, 50mA of H.T. current, the ripple

current in C1 would be approximately 150mA. On the other hand, if the circuit were supplying 200mA for an audio amplifier or television set, then the capacitor would have to be rated for a safe ripple current of at least 600mA.

It should be noted that there is a world of difference between capacitors with a ripple current rating of 150mA and 600mA, even though the working and surge voltages may be identical.

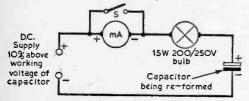


Fig. 3.—A suitable circuit for re-forming electrolytic capacitors.

Ambient Temperature

The ripple current rating is related to ambient temperature, since the power factor tends to increase with increase in temperature. If a capacitor which is unable adequately to handle the ripple current is employed as reservoir, its temperature will rise, and as a result its inadequate ripple current rating will be further reduced. Eventually, the capacitor will become so hot and pass so much ripple current that it will explode.

A test of this nature was carried out on a television receiver. The original reservoir capacitor was disconnected and in its place was wired a capacitor of the same value and voltage working but with a 150mA ripple current rating. The set worked perfectly when first switched on, but the capacitor quickly became hot. The temperature progressively increased, and without warning the component exploded with considerable violence. Fortunately, the set was set up with this in mind and was lightly fused, thereby saving the rectifier.

Multiple Capacitors

Electrolytic capacitors are made in units of two or more elements. In most cases there is a common negative terminal, or the can itself may be negative. The positive terminals are then colourcoded to correspond to the various capacitances as indicated on the outside of the case. The ripple current rating of most multiple capacitors is common to all elements, but where this is not the case, the section with the highest ripple current rating, which should be used as the reservoir, is generally indicated.

Some metal canned capacitors also have a negative terminal which may or may not be connected to the metal case. Where there is no connection between case and negative terminal, it is usually indicated that the can is isolated, and it is as well to ensure that the can remains isolated from H.T. negative or chassis in actual service. On the other hand, where the can is definitely connected to the negative terminal, then it is perfectly in order to

clamp the can directly to chassis.

Power Factor and Insulation Resistance

The power factor of a capacitor is a measure of the loss of energy which results when A.C. is

passed through it and is given by the ratio of watts (actually measured) to volt amperes. Power factors of the order of 15% are permitted with electro-lytic capacitors; a figure which could never be tolerated with paper and mica capacitors of the kind used in R.F. circuits.

A capacitor with a poor power factor will be found to have a relatively large leakage current. This can be dangerous since it results in overheating (owing to the poor insulation resistance) and may cause damage to the rectifier and

associated components.

It should be noted that it is normal for the leakage current to rise rapidly above the working voltage, as shown in Fig. 2, and it is this factor which endows an electrolytic with a surge rating.

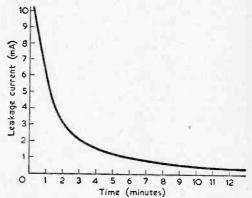
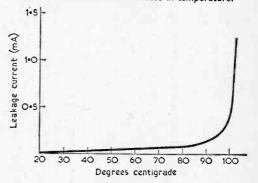


Fig. 4 (above).—The leakage current reduces with time in a capacitor which responds to re-forming.

Fig. 5 (below).—This graph shows how the leakage. current increases with increase in temperature.



For example, when first switching on a receiver the voltage across the electrolytics is above the normal working value, but since the leakage current is then higher than normal, the capacitors effectively absorb the direct current and thereby prevent the H.T. voltage rising to a level which may otherwise damage associated components. The surge rating in this respect is usually about 100V above the working voltage.

(Continued on page 611)

UNITS AN NSTABILITY By A. Sydenham

CURING FEEDBACK AND OSCILLATION

IMPLE radio receivers and tuners employing (tuned radio frequency) principles are favoured by many constructors as they are not so expensive to construct as A.M. superhets, F.M. or transistorised receivers. TRF front ends are used too by quality enthusiasts, for excellent results can be obtained from comparatively simple apparatus when the output is fed into a good quality amplifier. The really serious listener usually invests eventually in a VHF tuner, but owing to the cash outlay required for such a set, he must sometimes be content meanwhile with less complicated apparatus.

A TRF tuner for use with an amplifier or as an integral part of a receiver often comprises a single R.F. amplifying stage coupled to a detector, no reaction (positive feedback) being applied in the interests of quality. The intervalve tuned circuit is not much damped if a detector of the infinite impedance type is employed and selectivity is fairly good provided high grade coils are used. The overall sensitivity is of a low order, but is usually adequate for local station reception -which is all one obtains from VHF apparatus anyway!

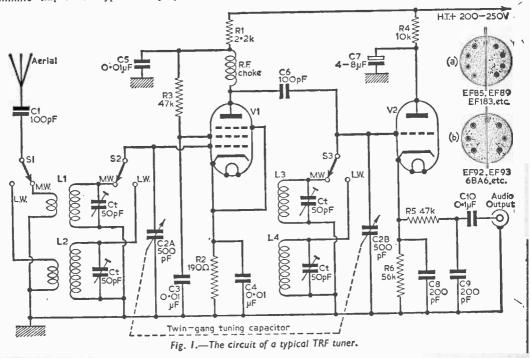
A Typical TRF Circuit

A basic circuit for a tuner is shown in Fig. 1 and it looks remarkably simple. Unfortunately, such tuners may prove very unstable and fierce oscillation that makes any form of listening impossible frequently results.

Such instability is usually most serious at the high frequency end of the band being tuned, i.e. where the tuning condenser vanes are least enmeshed—at the other end of the scale the gain tends to be less. Such oscillation is due to unwanted feedback from the anode of V1 to its grid (Fig. 1) and can arise in several ways, usually due to capacitative or electromagnetic coupling.

Tracing Instability

The cure is to find and remove each unwanted coupling and is not easy unless great care has



been paid to the initial layout and construction. Sometimes no feedback is evident until alignment is attempted, and only when the tuned circuits are brought to resonance by means of the trimmers provided for this purpose does howling commence.

There are several methods by which the R.F. valve may be coupled to the detector circuit, and in the circuit of Fig. 1, choke capacity coupling is depicted since this method simplifies switching and also ensures reasonably high gain together with a fair amount of protection against instability.

Fig. 2(a).—'Tuned anode' intervalve coupling.

winding

Tuned anode coupling gives greater gain but increases the risk of instability whilst aperiodic coupling, although ensuring excellent stability, tends to make switching complicated when several wavebands are to be incorporated in the tuner, as both the primary and secondary windings of the intervalve coils must be switched. The primary windings also carry H.T. supplies to the anode of the R.F. valve. The two forms of coupling may be seen in Figs. 2(a) and 2(b).

Essentials

If any wiring associated with the anode circuit of V1 or the grid circuit of V2 is allowed to run in close proximity to that of the input wiring to V1, positive feedback will occur. It is essential, therefore, to keep these circuits and their wiring as far apart as possible and to use earthed screening where necessary. It is very tempting to use a miniature, single wafer rotary switch for band changing, but a little thought will show that this is most undesirable as the interstage wiring must necessarily be in proximity at the contacts. A two-wafer type is essential, and each wafer should be separated from the other by spacers. If the aerial and intervalve coils are to be mounted in the same plane as the switch, screens should be incorporated as shown in Fig. 3. Usually, however, one set of coils can be mounted above the

chassis and one below, so that the chassis provides its own screen. Designers usually pay considerable attention to these points when developing a prototype model for construction purposes, and the beginner is well advised to use the specified components and to follow the layout given as closely as possible.

It is sometimes beneficial to fit a screen to the base of the R.F. valve as the pin layout usually permits the input and output circuits to be separated. Some bases are shown on the right-

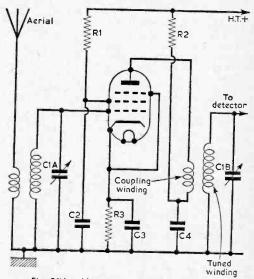


Fig. 2(b).—'Aperiodic' intervalve coupling.

hand side of Fig. 1, the double line indicating the screen position. Such screens may easily be made from tinplate and should be approximately §in. high. Careful orientation of the base in a

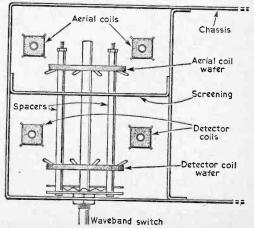


Fig. 3.—Avoiding instability by the judicious use of screening.

newly constructed tuner can also affect the length of the connecting leads considerably.

Curing Instability

In a receiver or tuner that has previously worked satisfactorily and then suddenly developed instability, the trouble is more than likely due to a component failure, and the usual tests should be made to isolate it. In newly constructed apparatus, however, capacitive or electromagnetic coupling

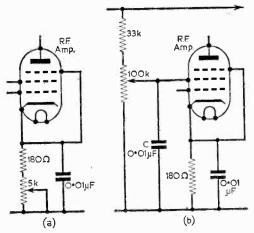


Fig. 4.—Temporary cures for instability—in (a), a 5k potentiometer is added in the cathode lead, and in (b), a 100k potentiometer is used to vary the screen grid potential,

should be suspected if oscillation and general instability is present, particularly if the trouble is worst at the high frequency end of the band being tuned. A temporary cure can usually be effected by connecting a 5000Ω potentiometer in series with the earthy end of the existing bias resistor as shown in Fig. 4(a). Alternatively a 100k potentiometer may be fitted in series with the screen feed resistor as shown in Fig. 4(b), but in this case care must be taken to see that the screen bypass condenser, C, is in direct connection with the screen grid pin tag rather than the slider

of the potentiometer. Adjustment of the control will lower the gain of the valve, and it should be set so that any unwanted oscillations just cease. The next step is to align the tuned circuits, and this will inevitably mean readjusting the newly fitted potentiometer to obtain stability. With the unit adjusted to the very edge of oscillation it should be possible to tune in a transmission, but good results cannot be expected as the R.F. valve is unlikely to be performing at its best owing to the incorrect voltages being applied. With the receiver or tuner in this state, it is usually possible to find the offending lead or leads by prodding the wiring with an insulated tool such as a discarded knitting needle, when the faulty lead will be evident as oscillation suddenly occurs. Several leads may be involved and these should then be screened, the screening being earthed at both ends. Although the work will prove tedious it is well worthwhile.

The potentiometer will need adjustment from time to time as improvement results and, finally, may be removed from the circuit entirely, when full gain conditions have been realised.

Another source of instability may be the twin gang tuning condenser, and this should be checked to ensure that good contact is made with the chassis at several points. The detector circuit also can be responsible for feedback difficulties and, referring to Fig. 1, it will be observed that the demodulated signal is taken from the cathode of V2 and then passed through a filter comprising R5, C8 and C9, which is intended to remove any residual unwanted R.F. accompanying the audio signal. Since no filter is perfect, it is possible for a small amount of this R.F. to pass via the output circuit back to V1 and give trouble. A good "in-line" layout will usually avoid this, however, but in difficult cases a suitable choke should be fitted in place of R5. The decoupling capacitor C8 is also critical; if it is low in value, uncontrollable oscillation may result. It may easily be checked by wiring another condenser in parallel.

Creating Instability

In conclusion, it should be noted that benefit is sometimes derived by making a hitherto stable TRF tuner slightly unstable deliberately to

increase gain.

As mentioned earlier, reaction is undesirable in modern equipment, but the use of a judicious amount of feedback can improve sensitivity. This may be obtained by soldering a short, insulated length of connecting wire to each of the fixed plate sections of the twin gang tuning condenser. The receiver or tuner should now be switched on and tuned to the high frequency end of the scale, when the wires, not bared, are twisted together until oscillation commences. They should then be shortened and untwisted carefully until oscillation just ceases. The extra gain is, unfortunately, not constant, over the whole range of tuning but, as no extra control is needed, the inclusion of the device is sometimes worthwhile.

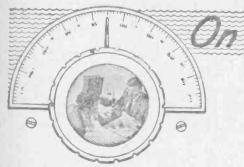
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Copies of this Standard may be obtained from the British Standards Institution. Sales Branch, 2, Park Street, London, W.1., price 5s. each. (Postage will be charged extra to non-subscribers.)



Those Transistor Sets!

N the October issue I made some further comments on the abuse which is being made of these small portables, and gave some details of an idea which had been sent to me by a reader. This hinted that an interfering set could be made with a very limited range to "jam" the annoying receiver. As I mentioned, and as I expected, the authorities do not look with any favour on this idea and the following remarks have been received from the G.P.O. "... under the Wireless Telegraphy Act, 1949, it is an offence deliberately to interfere with any form of wireless telegraphy (which includes broadcast receiving apparatus), either by wireless telegraphy or electrical apparatus". The relevant part of the Act is section 13 which states:—"Any person who uses any apparatus for the purpose of interfering with any wireless telegraphy shall be guilty of an offence under this Act. The penalty on conviction for such an offence is imprisonment for a period not exceedofficies in fingisonment for a period not exceeding one hundred pounds, or both.". The Postmaster General could not, therefore, sanction the use of any equipment designed for the purpose suggested. So if any reader is thinking of making up a unit on the lines suggested, my advice is "don't". The letter from the GPO goes on to say however that from the G.P.O. goes on to say, however, that "Undue noise caused by the excessive use of a loudspeaker is in a similar category to that caused by the inconsiderate use of a musical instrument, for example, and Local Authorities already have power to make bye-laws for the prevention and suppression of such nuisances". I note that it was recently reported that the Eastbourne council desired to make such an additional bye-law and, as this has to be approved by the Government, application was made but the council was informed that permission could not be given as the position of these portable receivers was being considered at Government level and an announcement would be made in due course.

Old-time Equipment

A number of readers have written recently extolling the virtues of old equipment which they remember owning, and in many instances have said that they are quite certain that the results were better than present-day equipment. I wonder if this is really so, or whether their memories have not been dulled by the passage of time?

BY THERMION

our Wavelengt

I do remember a well-known reverend gentleman who used to write for us, who was also an authority on the organ, and who was a very keen experimenter, but many of the circuits he tried and extolled had no technical measurements or other data which we could now refer to, in order to see whether their performance was good or not. One of his circuits had many very good claims which were upheld by a host of readers judging by the letters we received. This utilised two high-class L.F. transformers (Eerranti products) coupled in a series-parallel arrangement, and his claims for bass reproduction as shown by organ reproduction were remarkable. Perhaps there are still some readers who are using this coupling, although L.F. transformers are not now available.

Remote Control

I was intrigued by the remote control devices shown at this year's Radio Show. I think I liked best the beam of light idea used to switch on and off a TV receiver, and also to change stations. I think I have remarked before, that one of our early contributors suggested, many years ago, that eventually the radio and TV would be consigned to the cellar together with the normal electric and gas meters, all listening or viewing being carried out by remote controls. There was at one time on the market a neat relay switch, operated by a drycell, which was fitted next to the radio, and pushbuttons suitably sited in every room permitted a receiver, even of the mains type, to be switched on or off from any room in the house. A simple modification of this would permit station changing, and I wonder this has not come into more general use. It would enable a really good speaker cabinet to be designed to suit the room furnishings.

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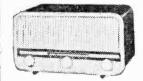
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Short-wave Listeners' Log

HEN an ordinary domestic or similar receiver is the only one available, it is usually impossible to cover the 160m and 80m amateur bands, which are often very interesting. Many popular receivers tune approximately 1000-2000m (3001150kc/s) on the long wave range, 200-550m (1500-550kc/s) on the medium wave range, and may have a single short wave range of about 19-45m (16-6.5Mc/s). There is thus a wide gap from about 45-200m (6.5-1.5Mc/s).

Some receivers can be made to cover the 160m band, with no modification other than unscrewing the M.W. band trimmers. This band extends from 1.8-2Mc/s (roughly 170-150m) and should be reached with the gang condenser almost fully open. It may be necessary to remove the trimmers entirely, or replace them with low-capacity trimmers. The receiver should be realigned, and will give similar M.W. results as before, though

dial readings will no longer apply.

Quite often the L.W. band is little used. With home constructed receivers, it is then relatively easy to fit coils for about 70-170m (4:25-1:8Mc/s). this will allow both 80m and 160m bands to be covered. If the L.W. range is to be retained, it will be necessary to replace the existing wavechange switch with one having an additional position. The new coils should be of the correct have an intermediate Most receivers frequency of around 465kc/s, and aerial and oscillator coils for this can easily be obtained. only other additional components required will be a 50pF or similar trimmer for each coil, and the oscillator coil padder.

Many ordinary receivers will give good results on these bands. A new tuning scale should be

drawn up to suit.

M and A Calls

New listeners on the amateur bands may be puzzled by the use of the letters M and A, which may be added to ordinary call signs. The letter M denotes a Mobile station, for example, one fitted in a car. Quite a number of such stations are in operation, especially at week-ends and holiday periods. The letter is added at the end of the usual call. For example, G3ZZZ/M.

The letter A shows that the station is being operated from an alternative address. That is, the operator has some kind of transportable equipment, which he has taken away from the usual station. When working in this way, the call would be G3ZZZ/A. Any station may operate in this way, whenever wished, but the locality must be announced at intervals. It is thus easy to log the place from which a /A station is transmitting.

Station Logging

When logging stations received, it is useful to employ the readability and signal strength code.

which will give a good indication of the results obtained.

Readability is from 1 to 5, as follows: Unreadable.

Barely readable, occasional words distinguished.

Readable with considerable difficulty. Readable with practically no difficulty.

Perfectly readable.

Signal strength is from 1 to 9, as follows:

Barely perceptible signals.

Very weak signals. Weak sig....ls.

Fair signals.

Fairly good signals. Good signals.

Moderately strong signals.

Strong signals.

Extremely strong signals.

A signal that is 5/9 is thus perfectly readable, and very strong. A 4/3 signal would be weak, but readable. A 2-3/5 signal would be fairly strong. but only readable at its best with difficulty, due to interference or other causes.

Times are best logged in G.M.T. This simply begins at 1a.m. and goes right through to 24, or midnight. For example, 8:10a.m. would be 08:10 G.M.T., or 0810 G.M.T. Similarly, 2p.m. would be 14:00 or 1400 G.M.T., while 11:40 p.m. would be 2340 G.M.T., and so on. When British Summer Time is in use, one hour has to be deducted, to obtain normal time. So 11:00a.m. B.S.T. would be 1000 G.M.T.

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FAULTS IN VHF/F.M.

1-The aerial and tuner unit

By G. J. King

LMOST the whole of the British Isles is within range of the VHF/F.M. service, and the majority of radio receivers now produced cater for such reception-including certain transistorised portables and television receivers.

The circuitry and characteristics of these receivers differ from A.M.-only sets, and one of the most obvious differences is in the aerial required. Unlike the ordinary "long-wire" or untuned aerial which works admirably with ordinary A.M. receivers, F.M. receivers require something a little more elaborate in the way of a tuned aerial if the best reception is to be obtained. The modern F.M. receiver or tuner is highly sensitive, and for this reason will give a useful A.F. output in all but extreme fringe areas on a short length of wire. Unfortunately, many sets are, in fact, operating under such conditions, and the reception as a consequence is no better, and sometimes worse, than that obtained by the A.M. services. Listeners have rightly been led to believe that F.M. reception is better than A.M. reception, and they are justly disappointed when they find in practice that this is not always true. The trouble, of course, is usually the aerial system.

Effects

A sensitive receiver often encourages the experimenter to make do with an aerial of dubious characteristics and performance, simply because the aerial provides a signal sufficient to give an audible output signal. This is not enough unless one lives very close to a transmitter, and even then, a poor aerial may cause an interference effect. The very quiet background which F.M. can provide, and which can be so impressive in comparison with A.M. reception, cannot be obtained with a weak acrial signal.

The noise suppression inherent in F.M. only works properly when the signal strength is above a certain level, and it usually follows that the stronger the signal the better the noise suppression and the quieter the background. This applies particularly to electrical and car interference, for even though the set may be tuned accurately, such interference disturbances may break into the programme if the aerial signal is of insufficient

strength.

Multipath Interference

Multipath interference can also be extremely troublesome and disconcerting, especially if insufficient attention has been given to the aerial. This interference is the result of the receiving

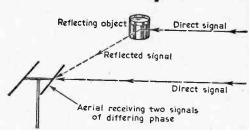


Fig. 1.—The cause of multipath distortion: the aerial picks up two signals of differing phase since the reflected signal arrives later than the direct signal.

aerial picking up two signals from the same transmitter. One is the direct signal from the transmitting aerial and the other is an indirect signal which has been reflected by an object such as a gas-holder, large buildings hills, or even trees. The effect is shown in Fig. 1, and the indirect signal arrives a fraction of a second later at the receiving aerial than the direct signal. This means that the indirect signal will arrive out of phase with the direct signal and a modulation owing to the phase difference will be produced.

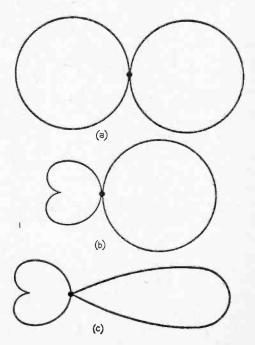


Fig. 2 (a).—The polar response of (a) a simple horizontal dipole; (b) a horizontal dipole with reflector and (c), a dipole with reflector and director.

RECEIVERS

Although an F.M. receiver is insensitive to amplitude modulation, it is, in fact, sensitive to phase modulation, since this is very much like frequency modulation. Thus, owing to the phase modulation produced by the reflected signal, a form of distortion is produced, which is sometimes called "multipath distortion".

Distortion

The resulting deformation of the programme material is difficult to assess and varies depending on the strength and phase difference of the reflected signal or signals in relation to the direct signal. In most cases a buzz or rattle distinctly spoils the reception, which in certain instances may be mistaken for audio distortion or an out-of-centre loudspeaker. This can usually be proved, however, by tuning to another programme as the trouble is rarely consistent on all programmes.

Passing aircraft may give similar symptoms during the time that the aircraft is close enough to act as a reflector. A bcat effect accompanied by distortion occurs as the direct, and reflected signals are received in and out of phase owing to the rapid movement of the reflecting surface. It will be realised that multipath interference is caused by the effect which causes "ghosting" on television pictures.

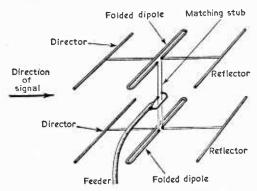


Fig. 3.—Two arrays stacked as shown increase the vertical directivity and reduce the distortion caused by reflections from aircraft.

The Cure

Where the distortion is severe, a cure can be effected by the use of a directional array orientated for maximum discrimination between the direct and reflected signals. In practice, this means a multi-element aerial, for a simple dipole cannot discriminate between the required signals and signals reaching the aerial from other directions. The addition of further elements to a simple dipole results in an increase of forward gain at the expense of gain in other directions. This effect is shown by the polar diagrams in Fig. 2. The diagram (a) is representative of the response of a

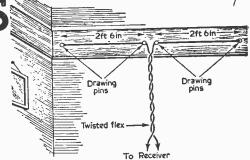


Fig. 4.—A simple indoor F.M. aerial, shown mounted on the picture rail.

dipole alone; (b) of the dipole with a reflector and (c) the dipole with reflector and director. From these it may be seen that (c) will obviously provide better discrimination than (a) or (b) between a signal arriving in the direction of the axis of the response and another at right-angles to it.

Vertical Directivity

Where multipath distortion is troublesome owing to passing aircraft, the only cure is to obtain improved directivity so as to provide greater discrimination between the low angle direct signal and the relatively high angle reflected signal.

This is possible by using two aerial systems, one above the other, as shown in Fig. 3. The two dipoles are in effect connected in parallel via a coaxial transformer or some other matching arrangement and then connected to the common coaxial down lead. This, then, causes the vertical polar response to become similar to the horizontal response of Fig. 2(b). The spacing of the two arrays has an effect on the vertical response, but a spacing between 4 and 5ft is usually about the best compromise.

Simple Aerials

Most modern receivers feature an internal "compressed" dipole made up of tin-foil or wire in the receiver cabinet. This is not of the correct length to tune the VHF band in itself, but is tuned by the use of a "loading coil" or similar device.

by the use of a "loading coil" or similar device.
In areas of strong signal such an aerial is adequate, provided there is not a lot of local electrical interference and the set is orientated for the best signal pick-up. However, where the internal aerial provides only mediocre reception, considerable improvement is usually possible by using a simple room or attic aerial.

In its simplest form, this consists of a length of ordinary electrical flex divided at the top to form two lengths of 2ft 6in., as shown in Fig. 4. The remainder of the flex is then used as the feeder or downlead to connect to the "dipole" sockets on the set.

Downlead

An improvement on this is to use proper coaxial or twin feeder downlead from the two dipole sections to connect the dipole to the set. Most sets require coaxial downlead to suit the tune;

input circuit, though earlier sets were designed for 3000 flat twin feeder.

This type of aerial has a polar response similar to that of Fig. 2(a) and is, therefore, somewhat directional which, theoretically, means that it should face the station broadside on. In practice, however, the wavefront tends to alter in direction owing to structures and, for this reason, the aerial should be positioned for the best signal-tonoise ratio. If local interference is excessive, then the only solution is to use a direction array of two or more elements mounted as high as possible outside the interference field.

The VHF Tuner

In most combined A.M./
F.M. receivers a separate
F.M. tuner sub-chassis is incorporated, a typical circuit of
which is given in Fig. 5.
Rather like the multi-channel
tuner of a television receiver,

the F.M. tuner is often independent of the main receiver chassis, but contains its own tuning arrangements which may or may not be ganged to the main A.M. tuning mechanism.

In other sets and in F.M.-only models, the tuner section may be built as part of the actual set on a common chassis. Nevertheless, the R.F. amplifier and frequency changer sections very closely follow the circuit of Fig. 5. Here, a double-triode valve functions in the first section as the R.F. amplifier and in the second section as a self-oscillating frequency changer.

Input Stage

The R.F. amplifier circuit differs slightly from set to set, for in some sets it may be arranged in the earthed cathode mode with neutralisation, as in Fig. 5, and in other sets as a grounded grid stage. There is possibly a slight gain advantage with the earthed cathode arrangement, but this cannot always be fully realised since the first tuned circuit is heavily damped to avoid the need for variable tuning.

In Fig. 5 the first tuned circuit, L3, is fixed-tuned by C3 and

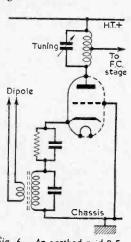


Fig. 6.—An earthed grid R.F. amplifier stage.

C4, and the aerial signal is coupled in by L2.

The anode tuned circuit, L4, is fixed-tuned

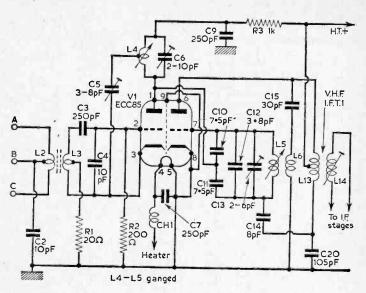


Fig. 5.—The circuit diagram of an F.M. tuner as used in A.M./F.M. receivers.

by trimmer C6 and permeability-tuned over Band II by a mechanically-coupled core in L4.

The dipole is coupled to L2 between points A and C when 300Ω feeder is Lsed. Point B may then be connected to the A.M. aerial socket to provide medium-frequency pick-up from the VHF aerial. When 75Ω coaxial is used, then point B is usually connected to chassis and connection made between A and B, with the outer braid to B.

Broad Tuning

The cathode resistor of the first triode is R1, and R2 is the damping resistor so that the grid circuit will tune reasonably flatly over the whole of Band II. The trimmer C5 is for neutralising the capacitance between the anode and grid of the valve (Cag). Without neutralisation, the internal Cag of the valve would cause positive feedback between the grid and anode circuits and the valve would act as an oscillator. The neutralising capacitor provides a negative feedback path which, when accurately adjusted, cancels out the positive feedback, and the stage is made inherently stable and thus works as an amplifier.

With grounded grid R.F. stages, neutralisation is not required since the input signal is fed to the cathode and the grid, being earthed, acts as an electrostatic screen and removes the effects of the internal capacitance. A grounded grid stage is shown in Fig. 6.

The frequency changer section of Fig. 5 is made up of the second triode, the oscillator coils, L5/L6, and the I.F. output transformer, L13/L14. L5 is also permeability tuned, and the core in this coil is mechanically coupled to the core in the R.F. coil L4. To avoid unnecessary coupling of the oscillator signal to the aerial, via the R.F. stage, the coupling from the anode of the R.F. amplifier is made to the frequency changer at the junction

of capacitors C10 and C11. At this point the oscillator voltage is almost zero, since it represents the null point of a bridge circuit.

Tuning Variations

Oscillator drift is a common trouble in F.M. receivers, and this causes the tuning point to alter progressively as long as the receiver is switched on. A certain amount of drift during the first five to ten minutes is quite normal, but prolonged drift should first lead to a check on the receiver ventilation. If the set is positioned too close to a wall or if the ventilation slots at the base and rear of the cabinet are not completely

clear, the temperature inside the set will become abnormal, making drift inevitable.

Dirty Valve Pins

A faulty valve or poor connections between the pins and the valveholder sockets is another cause. In obstinate cases, the trouble could be caused by a fault in one of the oscillator tuning capacitors. These are C10, C11, C12 and C13, and since they have a computed temperature coefficient, replacement must be made only with

components recommended by the makers. The positioning is also very critical, and the replacement component must occupy exactly the same position as the original.

Critical Layout

The tuner unit is usually screened by screw-on metal panels, and to avoid oscillator drift and microphony it is essential that these are secured tightly after a servicing operation. It is also important not to disturb unnecessarily the wiring in the tuner unit, as this could result in misalignment and also instability which could give the effect of microphony. In Fig. 7 is shown the inside of a tuner unit which employs permeability tuning. The permeability-tuned coils can clearly be seen, as also can the coil-springs which hold the cores under tension against the cord-drive arrangement.

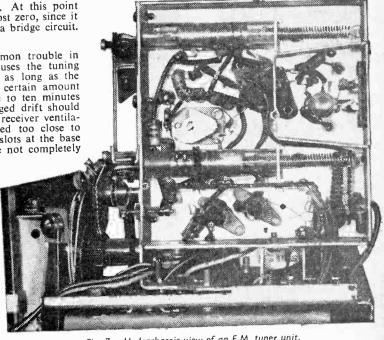


Fig. 7.—Underchassis view of an F.M. tuner unit.

The cord-drive is coupled to the main tuning mechanism, and as this is operated, so the cores traverse the coil formers to tune over Band II.

Fig. 7 also shows the components and the short connecting wires in relation to the valveholder. Microphony can sometimes be detected by knocking the tuner chassis sharply with the handle of a screwdriver, and in this event the trouble is often caused by a poorly soldered connection, or small capacitors or resistors touching the chassis or some other component. Loose screening plates or cans produce a similar effect, as also does a micro-phonic valve and faulty valveholder. The microphony is produced by frequency modulation of the local oscillator, which, of course, gives rise to an audio output from the detector.

(To be continued)

A SIMPLE CONDENSER BRIDGE

(Continued from page 588)

For example, say the range switch is set at 0.001 µF and the circuit resistance of the variable resistance is found to be 500,000 ohms. Then- $C = 0.001 \times 1,000,000$

> 500,000 $= 0.002 \mu F$

This measurement is very accurate provided good components are used together with a reliable ohmmeter. (The range switch pointer indicates the lowest capacity to be read on each range.)

By adding a dial and pointer to the variable resistance, it will, of course, be possible to cali-brate the instrument, but this can lead to inaccuracies as the dial would have to be rather

closely marked.

The standard terminals are used when it is desired to test a condenser which is either above or below the range of the instrument. Suppose 0.5 µF condenser needs testing. First, a similar condenser, but known to be accurate, and say of capacity 0.45 µF, is connected to the standard terminals. The range switch is now turned to S and the 0.5 uF connected to the test terminals in the usual way.

The formula would now be:- $0.45 \times 1.000.000$

Circuit variable resistance If the condenser is correct, the variable resistance circuit resistance will be 900,000 Ω .

Practical Wireless

HE circuit of the Mini-Amp is fairly conventional, but the method of construction uses no chassis, printed circuit or nuts and bolts. The finished unit measures $4\frac{1}{2}$ in. x $1\frac{1}{2}$ in. x $1\frac{1}{8}$ in. and the volume control (which incorporates the on/off switch) could be fitted over the front end of the tag strip although it has been fitted on an extension screened lead on the prototype.

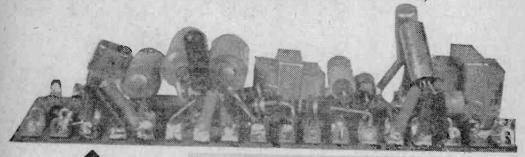
Current Consumption

The amplifier is designed to be fed from any conventional type of crystal pick-up and it is

possible to drive a 9V record-player motor from the same battery, although a separate battery is always best. The current consumption is about 4mA when switched on but not playing, and up to 50mA when playing, according to the volume. The amplifier will operate at full volume on one PP9 battery for 70 hours at least, at a cost of under 1d. per hour.

The components are definitely obtainable from any radio dealer to order and substitutes should not be used. The values of R10 and R11 are particularly important and 5% or 1% components

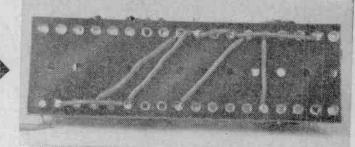
should be used (see Blueprint).

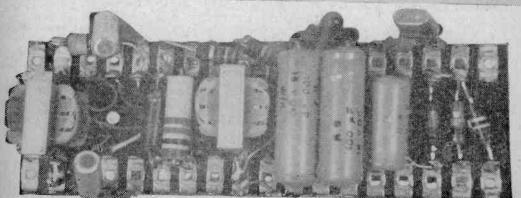


A General view of the Mini-Amp

The wiring on the reverse side of the group-board.

This shows clearly the simple layout of components.

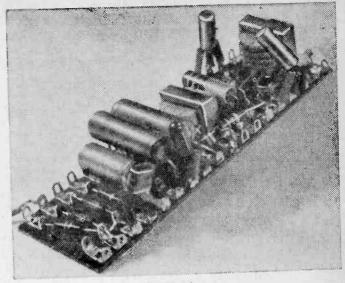




VIP

By J. Bisset

THE SECOND OF OUR PROGRESSIVE SERIES OF BLUEPRINT DESIGNS



The Mini-Amp.

Method of Construction

Full constructional details are given in the Blueprint, and wiring and assembly of the "Mini-Amp" should follow the layouts given in the correct order. The complete circuit diagram is given in Fig. 1 on the Blueprint, but it is not strictly necessary to understand this fully in order to build the "Mini-Amp". The first step in building the unit is to glue two strips of paper—

glue two strips of paper numbered as indicated in Fig. 2 to the group-board so that it will not be necessary to count the number of each tag to which the components have to be soldered. If glue is applied only at the ends of each strip, then they may easily be removed when construction is complete.

Mounting the Transformers (Fig. 3)

The two transformers are then mounted in the manner shown in Fig. 3. The fixing tags, which are bent under the transformers when they are purchased, are bent outwards, and the inner tags of the groupboard (17 and 35) are bent flat on the paxolin panel. Transformer T2 is then soldered in position with the side having two brown wires towards tags 18 and 36.

The other transformer (T1) is mounted on tags 10 and 28 in the same way with the two-wire side towards tags 1 and 19. The first stage of construction is now completed and should look like Fig. 4. The transformer leads are now shortened carefully so as to reach the tags shown. They are then carefully soldered to the tags exactly as in Fig. 4. The wires of miniature components are very fragile and care is

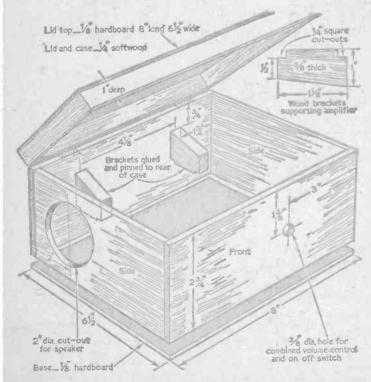
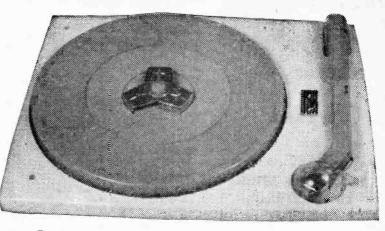


Fig. 11.—Details of a suitable cabinet for the Mini-Amp used in a record player.

required in removing the insulation if the wires are not to be severed within the transformers.

Fixing the Resistors in Circuit (Fig. 5)

The numbers in brackets on the components list are the tags to which the resistors are soldered. These can also be seen in Fig. 5 which shows the additional wiring to that of Fig. 4. Where wires solder to tags to which the transformers are mounted, do not use too much heat (tags 10, 17, 28 and 35). Keep the wires of all the resistors as short as possible and check that no solder falls between adjacent tags.



The record player deck used in this design (available from many advertisers and distributed in this country by Greencoat Electronics Ltd., 2 Princes Row, Buckingham Palace Road, London, S.W.1).

Fixing the Condensers in Circuit (Fig. 6)

The small condenser C1 is the first to be fixed in circuit between tags 22 and 26, it must be laid

And the state of t

Fig. 12.—Dimensions of the motor-board and cut-out.

almost flat on the paxolin, but care is required so that it will not touch resistors and leads. The other condensers are then fixed as shown in Fig. 6. Note the polarity, usually denoted by the positive ends having red markings or a red or black rubber washer. Condensers with insulating sleeves over

the metal case are best in this position as then they may be positioned close to the other components.

Wiring on the Back of the Group-board (Fig. 7)

Certain wires between tags are required and the layout is shown in Fig. 7. One red wire, one blue, and two black wires are required. The red wire is the conventional earth or chassis wire. The blue wire joins the emitters of the output transistors and the black wire is for the negative "H.T." line.

External wiring (Figs. 8 and 10)

Two leads are required for the 3Ω P.M. speaker (any size up to 10in. will work well, but a 3in. loudspeaker gives good results and is little bigger than the "Mini-Amp").

Connecting the Screened Cable

Screened cable consists of a plastic-insulated wire which is surrounded by a tubular, woven-wire screen, which, in turn, is insulated with a plastic covering. When making connections to screened cable, the first step is to expose the screening of the cable by stripping off about 1in. of the outer covering of the cable—taking care not to cut the fine wires of the screen in the process. Next, unravel the woven screen with a large needle or pointed object. When it is unravelled, twist the strands together so that they form a connecting wire separate from the inner wire (which should now be exposed). The insulation of the inner wire may now be removed for a length of about 4in. and the strands twisted together. The screening and inner wire are now ready to be soldered where required.

A screened lead is taken from tags 1 and 2 to the volume control, the *inner* lead going to the middle (slider) tag, and the screening of the cable is soldered to the tags shown in Fig. 8. A similar wire is taken to the crystal pick-up, the screening and inner lead being soldered as shown in Fig. 8.

The screening acts as one battery lead and is also connected to one tag of the switch, the other tag going to the positive battery terminal.

Fixing the transistors (Fig. 9)

The leads of the four transistors are cut to in. carefully and coloured sleeving slipped on. A suggested scheme is:-

Collectors — Black Bases — Green Emitters - Red.

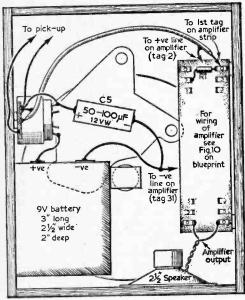


Fig. 13.—The wiring diagram of the record player.

The leads of the transistors should be soldered into circuit as quickly as possible so that the leads do not become too hot. A heat sink should be used to conduct the heat away from the transistors themselves as each lead is soldered into position. Complete details of the procedure, together with illustrations, were given on page 509 of the October issue in the article on the "Tutor". The method described used a pair of long-nosed pliers as a heat sink, but it is possible to use a small piece of damp cloth wrapped round the leads if care is taken not to allow other components to become

The complete layout is given in Fig. 10 and the wiring should be checked carefully against this diagram before testing the unit. It is most important that all components have been connected correctly, especially the condensers and transistors. The battery must be connected correctly or the

transistors will be ruined.

The transistors may be bent over gently so as to take up less space, but the leads should not be bent nearer than in. to the transistors.

The completed layout is shown in Fig. 10.

Using the Mini-amp

The ideal use for an amplifier of the small size of the Mini-Amp is in a battery-operated, record player. A suitable turntable unit can be seen in the illustration (page 610). This deck is for playing 45rev/min records—EP's—and it can be powered from the same battery as the Mini-Amp, provided that a condenser of 100 µF 12VW is wired across the "H.T." line of the amplifier and motor. This condenser prevents any interaction between the motor and the amplifier, and is clearly shown in Fig. 13. This condenser must not be wired on the battery side of the on/off switch or excessive battery drain may may take place. The dimensions and construction of a suitable case for the record player are shown in Fig. 11, and the small size of the finished unit is illustrated. The case is of simple box form and has a hinged lid; when finished, it may be covered in an adhesive plastic material or rexine if desired. The dimensions of the motor-board are given in Fig. 12, and an underside view of the record player in Fig. 13—this diagram also shows the simple wiring needed to link up the deck with the amplifier.

The loudspeaker recommended for the EP record player is the 2½in. Whiteley model P2.585. It should be noted that the leads of the gram motor are taken from battery negative and the on/off switch so that the switch functions for both

the Mini-Amp, and the motor.

Next month's article and free gift Blueprint will deal with the construction of a superhet frequencychanger and I.F. amplifier of which the Mini-Amp will form the output stages.

Electrolytic Capacitors

(Continued from page 596)

Capacitors which have been stored for any length of time may well suffer from a relatively high leakage current, but before they are thrown away an attempt should be made to re-form them. This is accomplished by connecting the capacitor across a D.C. supply giving a voltage approximately 10 per cent in excess of the working voltage of the capacitor. A 15W 230V bulb should be connected in series with the circuit, as shown in Fig. 3 (page 596). The current should be measured on a milliammeter, and for the sake of safety it is desirable to shunt the movement by a switch as shown by S.

Before switching on, S should be closed, and when the power is applied the bulb will glow fairly brightly to start, but will quickly dim right down and eventually go out as the capacitor re-forms. At this stage it will be safe to switch in the milliammeter, and the resulting reading will represent the leakage current of the capacitor.

If the bulb or bulbs light brightly and remain so, then the capacitor is useless. if the bulb lights momentarily at random intervals during the re-forming process, the capacitor has an intermittent short and should not be used. The curve in Fig. 4 gives some idea how the leakage current will diminish with time in a capacitor which responds normally to treatment.

It should be noted that temperature increase affects the leakage current, and a curve illustrating

this effect is given in Fig. 5.

High A VERSATILE UNIT WITH VERY LOW NOISE AND DISTORTION LEVELS By R. Murray-Shelley Gain Amplifier

HE high sensitivity of this amplifier, together with its lack of distortion and low noise level, makes it suitable for use where a low input (such as is obtained from certain types of record player pick-up units, and the majority of tape playback heads) is available. The output of the amplifier is more than adequate for domestic purposes.

The Circuit

A novel feature of the circuit, the complete diagram of which is shown in Fig. 1, is the provision of both high and low input impedance facilities. In the normal way, a low impedance supply is matched to the naturally high input impedance of the valve amplifier using a matching transformer. This method has drawbacks, in that the transformer, unless it is very carefully screened, both electrically and magnetically, is a source of hum. In this circuit, therefore, a transistor is used to replace the matching transformer. It is connected in such a way that, while its input impedance is low, its output impedance is sufficiently high to match the valve amplifier. This circuit has the added advantage that the transistor provides a considerable amount of gain.

The remainder of the circuit is fairly conventional. Three amplifying valves are used. The first is an EF86 working as a voltage amplifier. This valve is particularly suitable in this position owing to its freedom from microphonic effects. This is resistance/capacity coupled to the following stage, a 6BR7—the 6BR7 is a B9A-based version of the better known octal-based 6J7, which could equally well be used in its place. The output stage comprises a single EL84, which is quite capable of giving up to 4½W output.

Feedback

Volume is controlled in the normal manner, by attenuating the input to the EF86 as required. A simple, but none the less effective, top-cut treble control is taken from the anode of this valve.

Negative feedback is used within the amplifier, both to reduce distortion, and to stabilise the operation of the unit. The main loop is taken from the secondary of the output transformer to the cathode of the 6BR7. This circuit is frequency selective, and by using a variable resistor in the loop as shown, control may be exercised over the bass response of the amplifier. This serves as a very efficient bass control circuit. A second negative feedback loop is between the anodes of the EF86 and the 6BR7, via a 2.2M resistor.

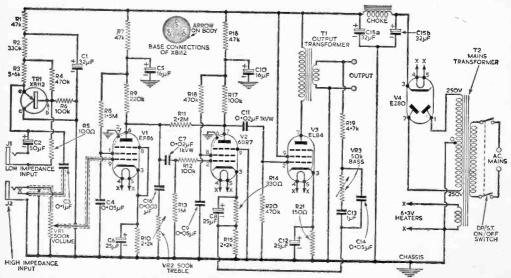


Fig. 1,—The circuit of the amplifier.

Power Supplies

It is very important when designing equipment of this kind, to ensure that adequate smoothing circuits are provided. This is particularly true, when, as in the case of this amplifier, the signals handled by the earlier stages are of a low magnitude. To this end it has been found necessary to decouple each stage using fairly high value electrolytic condensers.

The power unit itself is conventional. An EZ80 rectifier was used in the prototype, but almost any

valve, preferably having an indirectly heated cathode, could be used. The mains transformer should be capable of supplying 250-0-250V at 65-70mA, and 6.3V at 1.5A for the valve heaters. If a rectifier having a 5V heater is used, then provision must be made for this when obtaining the mains transformer.

The transistor obtains its power from the smoothed H.T. line, thus eliminating the need for any form of battery.

Components

The transistor used in this circuit is the XB112, and it is recommended that this specific component should be employed. The resistors in all cases need only be of 10% tolerance, and they should be rated at $\frac{1}{2}W$, with the exception of the cathode resistor, R21 (150 Ω), which should have a rating of at least 3W.

The output transformer should be capable of handling 5W. If a 3Ω impedance speaker is to be used with the unit, then a transformer ratio of 40:1 will be

required; for a 15Ω speaker, the ratio is 15.5:1.

The coupling condensers (C7 and C11) should be of 1,000VW D.C., and beyond suspicion as regards leakage. The valveholders, all B9A types, should, if possible, be of moulded or nylon loaded construction, to minimise the possibilities of breakdown or tracking.

It will be noticed from the circuit diagram (Fig. 1) that connections are made to the amplifier using jack plugs and sockets. Two jack sockets will be required for the inputs. One of these has

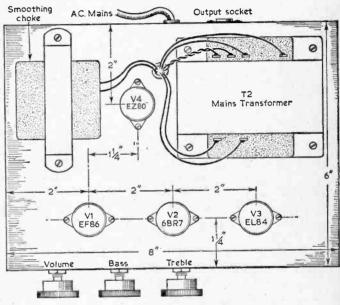


Fig. 2.—The above chassis layout of components.

			COMPONE	NTS LIST
Resisto	rs			CI3 I µF I50VW CI5 32+32 µF 450VW
RI R2 R3 R4 R5 R6 R7 R8 R9 R10	47k 330k 5·6k 470k 100 Ω 100k 47k 1·5M 220k 2·2k 2·2M	R12 R13 R14 R15 R16 R17 R18 R19 R20 R21	100k 1M 330 Ω 2·2k 47k 100k 470k 4·7k 470k 150 Ω 3W	C14 0.05 μF 250VW C16 0.003 μF 500VW VRI 500k potentiometer—log with D.P. switch VR2 500k potentiometer—linear JI Jack socket (Bulgin type JII) J2 Jack socket (Bulgin type JI2) T1 Output transformer (see text) T2 Mains transformer—Primary to suit main: supply Secondary, 250-0-250 T0MA 6-3V 1-5A
Capac CI C2	itors 32 μF 350VW 50 μF 25VW	C7 C8	0·02 μF 1,000VW 25 μF 25VW	VI EF86 V3 EL84 V2 6BR7 V4 EZ80
C3 C4	0·İ μF 250VW 0·05 μF 500VW	C9 C10 C11	0·05 μF 500VW 16 μF 350VW 0·02 μF 1000VW	TRI XBII2 transistor. Chassis, connecting wire, B9A valveholders
C5 C6	16 μF 350VW 25 μF 25VW	CIZ	25 μF 25VW	output socket, tagboards, etc.

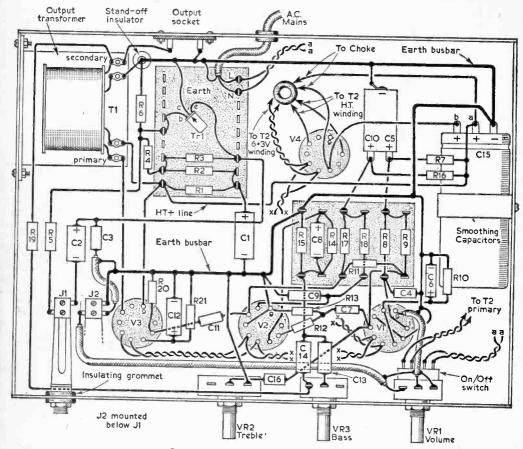


Fig. 3.—The underchassis wiring diagram.

integral switching contacts, which open the circuit when a plug is inserted. Thus, the effect of these contacts, when connected as shown, is to switch out the transistorised stage of the amplifier when a high impedance input is connected.

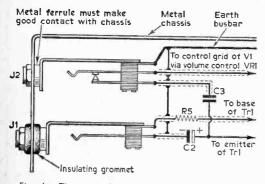


Fig. 4.—The method of mounting the jack sockets and the connections to them.

Construction

The prototype amplifier was built on an aluminium chassis, size 8in. x 6in. It would be impractical to use a chassis of smaller dimensions than these. On the other hand, the use of a very much larger chassis is not to be recommended, since all connections should be kept as short as possible to reduce the effects of induction and feedback which lead to noise and instability.

With a view to keeping down the hum level of the amplifier, all earth returns are made to an earth bus-bar, which is itself connected to the chassis at only one point. This bus-bar is made from a length of 16 or 18s.w.g. tinned copper wire, which is mounted on the chassis in the manner shown in Fig. 3.

The chassis itself is earthed. If it were left "floating", i.e. not connected to earth, then trouble might be experienced due to hum.

Mounting Components

It will be seen from the diagram (Fig. 3) that the output transformer is mounted below the chassis. This transformer is mounted first, (Continued on page 622)

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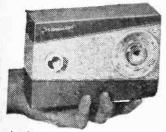
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By J. B. Dance, M.Sc.

HIS unit is a device which provides either greatly increased or greatly decreased amplification over a chosen narrow band of frequencies with a fairly level response over the remainder of the audio frequency spectrum. The frequencies in the chosen band are said to be either "selected" or "rejected".

Uses

Such a device is useful in 'phone reception when switched to the "reject" position because a narrow band of frequencies can be tuned out so as to remove a heterodyne whistle with negligible effect on other audio frequencies.

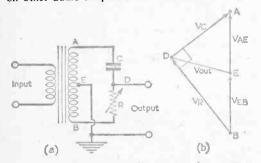


Fig. 1(a).—Simple circuit for variable phase output. Fig. 1(b).—The voltage vector diagram for the circuit of Fig. 1(a).

In C.W. reception the wanted audio beat note can be selected from all other audio frequency noise by using the instrument in the "select' tion where positive feedback is applied. If the amount of positive feedback is increased, oscillation will occur and the device can be used as a variable frequency audio oscillator which gives a constant output voltage as the frequency is altered.

Principle of Operation

Let us first consider the circuit of Fig. 1(a). The voltages at the points marked A and B are in

push-pull so that VAE=VEB where VAE is the voltage between points A and E. If the current taken from the output is negligible, the voltages in the circuit of Fig. 1(a) can be represented by the simple vector diagram of Fig. I(b) in which Vc=voltage across the condenser C and Vc=voltage across the condenser C and VR=voltage across R. The voltages Vc and VR are 90° out of phase and therefore the angle between them in the vector diagram is a right angle. From geometry it can be seen that as VR varies with R, the path traced out by the point D is a semi-circle of which E is the centre. Therefore the length of ED is constant but changes in direction. This means that the output voltage from the circuit of Fig. 1(a) is constant in amplitude but changes in phase as R varies. At one particular value of R (where ED in Fig. 1(b) is perpendicular

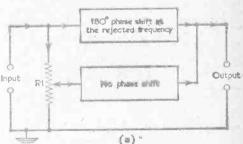


Fig. 2(a).—Block diagram of the filter unit switched to "reject".

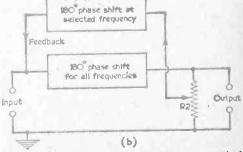


Fig. 2(b).—Block diagram of the filter unit switched to "select".

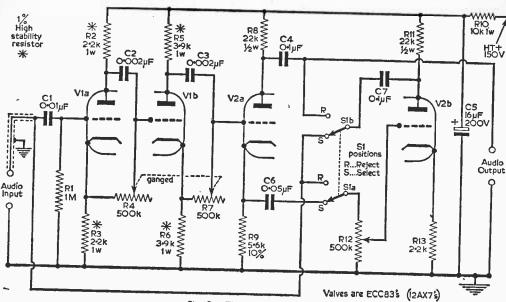


Fig. 3.—The series filter unit.

to AB) the output from Fig. 1(a) circuit will be 90° out of phase with the input at a certain frequency. Two such circuits in series can be used to obtain a phase shift of 180° at that frequency, the two variable resistors R being ganged together. At the frequency concerned the impedance of the condensers C will each equal the resistance of either of the resistors.

The block diagram of Fig. 2(a) shows how the arrangement discussed above can be used to give the rejection property of the filter. The audio input is applied to the circuit which will give 180° phase shift at the chosen frequency and is also applied via the potentiometer R1 to an amplifier which gives no phase shift (or alternatively 360° phase shift). If the potentiometer R1 is adjusted so that the gain of both the paths is the same, the two outputs will completely cancel at the chosen rejection frequency. At other frequencies the phase of the signal in the upper path will not be altered by 180° and cancellation will not occur at the output.

By simple switching the arrangement may be converted to that of Fig. 2(b); in this form a certain frequency can be "selected" or the circuit can be used as an oscillator. At the chosen frequency the upper amplifier gives 180° phase shift and the feedback is positive. The amount of feedback is determined by the setting of R2. If enough feedback is used, the unit will oscillate at the frequency at which the phase shift in the upper network is exactly 180°.

Practical Circuits

A practical circuit is shown in Fig. 3. It is not convenient in practice to use the transformer phase splitter circuit shown in Fig. 1(a) and cathode follower phase splitters are used (VIa and VIb in Fig. 3). The frequency determining components

are R4, C2 and R7, C3. Resistors R4 and R7 are ganged together; slight tracking errors in the ganging of these variable resistors is of practical importance, as it does not affect the amount of attenuation of unwanted frequencies. The valves used are two ECC83 or 12AX7 miniature high impedance double triodes. Two 6SL7 valves would give somewhat similar results and could be used if octal valves are preferred. In order to obtain the best results, R2 and R3 should be high stability components matched to each other to within ±1per cent. The same requirement applies to R5 and R6. Although the power dissipated in these resistors is not large, it is advisable to use 1 or 2W components, as these will tend to retain their values better than the smaller types. The resistors recommended are fairly small in value so that the output impedance of each circuit is small and the circuit is not therefore affected by the very small currents taken by the succeeding valves. The cathode resistors R3, R6 and R9 have been made progressively larger so that direct coupling can be employed between the stages (this reduces unwanted phase shift, but the cathode bias of each stage is applied to the grid of the succeeding stage).

In the "reject" position, R12 may be adjusted for maximum rejection of the unwanted signal. In the "select" position it should be adjusted to give the desired amount of emphasis to the wanted audio frequency. If it is advanced too far, oscillation will take place

lation will take place.

If the ganged components R4 and R7 are of the linear type, the frequency scale will be crowded at one end. An inverse semi-log type will give a scale which is much more evenly spread out. A 2-pole, 2-way rotary switch is required for S1 and S1b. In the position marked "S" in Fig. 3,

(Continued on page 621)

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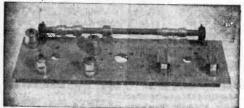
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the circuit is in the "select" position whilst in the position marked "R" it is in the "reject" position.

Use in Receivers

The values shown in the circuit of Fig. 3 have been chosen so that the output voltage is about the same as the input voltage. The unit can therefore be inserted in the receiver audio chain without affecting the gain of the receiver appreciably. It should normally be placed at a low level, high impedance point. Usually it is best to disconnect the diode detector in the receiver from the succeeding audio stage; the output from the detector is then fed into the unit and the output from the unit into the first audio stage of the receiver. This method of connection does not apply to the shunt circuit of Fig. 4 which is described later. If it is desired to obtain a gain of more than unity, the resistors R8 and R11 may be increased in value several times.

The frequency coverage is about 200c/s to 7kc/s. If a lower limit of about 75c/s is required, C2 and C3 should be increased in value to about $0.004\mu F$ or alternatively the resistance of the ganged variable resistors (R4 and R7) can be doubled to 1M each. If operation at high frequencies is desired, the values of C2 and C3 may be reduced to between 500pF and 1,000pF.

The H.T. supply should be well smoothed or H.T. fluctuations may cause the unit to oscillate when being used in the "select" position. A stabilised H.T. supply is, of course, ideal.

The Shunt Circuit

The circuit of Fig. 3 must be placed in series with the receiver audio circuit between, say, the

detector and the first audio stage. This is not always easy in practice and therefore the shunt circuit shown in Fig. 4 has been evolved. Only a single connection (other than the power supplies) is required between the receiver and the unit. The input to the unit is connected to the output of the receiver detector, but the detector is not disconnected from the following audio stage. The shunt circuit may therefore be connected to an existing receiver much more easily than the circuit shown in Fig. 3. A single coaxial connection may be used from the detector output so that the unit can conveniently be placed with its controls on the front panel. The input to the unit must be taken from a point of high impedance; this is normally the output of a diode detector, but if a cathode follower detector is used, a 220k resistor should be inserted immediately after the detector.

Signals of any undesired audio frequency are shorted to earth by the shunt unit when in the "reject" position, but, in the "select" position, the signals of the chosen frequency are greatly

amplified by feedback.

Low impedance miniature 12AU7 double triodes are used in the Fig. 4 circuit, but 6SN7 octal based valves will give a similar performance. V1b and V2a are the cathode follower phase splitters. The resistors R5 and R6 should be matched to ±1per cent. tolerance and should be high stability components. The same requirements apply to R11 and R12. A 6-pole, 2-way rotary switch is required for "select"/" reject" and it should have at least two wafers to avoid in-

stability problems.

The ganged variable resistors R14 and R10 determine the frequency of operation. The tracking need not be perfect.

(Continued on page 650)

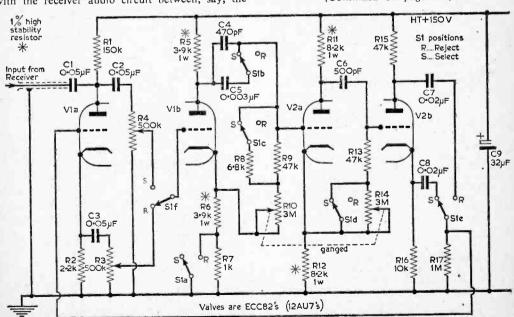


Fig. 4.—The shunt filter unit.

Club News

AMATEUR RADIO MOBILE SOCIETY

Hon. Sec.: G3FPK, 79 Murchison Road, London E.10.
Many A.R.M.S. members attended the National Mobile Rally on

September 10th at Woburn Abbey, Bedfordshire. Amongst other items, the competition for the Mobile Measurements Trophy was run. On September 24th the Surrey Radio Contact Club's 2 metre D.F. hunt was held.

DERBY AND DISTRICT AMATEUR RADIO SOCIETY Hon. Sec.: F. C. Ward, G2CVV, 5 Uplands Avenue, Littleover, Derbyshire.

over, Derbyshire. in connection with the Golden Jubilee Year celebrations the society have co-operated with the Museum authorities in the presentation of an exhibition covering fifty years of wireless. The exhibits include apparatus constructed in 1911 by members of the Derby Wireless Club. On September 6th the society held a surplus sale and on the 13th of the same month a direction finding practice run was held. Also during September members took part in the direction finding contest for President's Trophy.

Future Event:
October 11th—"The History and Development of Electric

Storage Battery."

GOSPORT AND DISTRICT AMATEUR RADIO CLUB Hon. Sec.: D. J. Gilbert, G3OYL, 45 Queens Road, Gosport,

Hampshire.

The first meeting on September 4th of this newly formed club, was held at the Gosport Community Centre, Bury House, Bury Road, Gosport. The club will meet every Monday evening at this address, at 7.30 p.m. A varied programme has been drawn up to cater for most aspects of amateur radio and anyone interested is welcome to attend the meetings.

It is hoped to have a club station operating at most meetings and ff possible a simple constructional course will be held for beginners.

GUILDFORD AND DISTRICT RADIO SOCIETY Hon. Sec.: J. R. Barker, G3PDX, 35 Banders Rise, Merrow, Guildford, Surrey.

At the moment many members are away on holiday but those who attended the meeting on September 14th heard a talk and discussion on S.S.B.

HOVE AND DISTRICT RADIO CLUB Hon. Sec.: E. M. Large, School House, Frout Road, Hove 4,

This new radio club holds its meetings every Wednesday from 7 to 9.45 p.m. at the Marmion Centre, Marmion Road, Hove 3. Anyone interested in any branch of amateur radio is welcome to attend the meetings.

MALMOE DX CLUB

This Swedish club invites DX-ers and short-wave enthusiasts in Britain to communicate with its members. Full details of che club, which caters for both SWL's and amateurs can be obtained from G. Traynor, 52 Kilbarchan Road, Johnstone, Renfrewshire, Scot-

MITCHAM AND DISTRICT RADIO SOCIETY
Hon. Sec.: M. Pharaoh, G3LCH, I Madeira Road, Mitcham.
Meetings of this society are now only held once every fourteen
days. This means that the club station meetings will be discontinued.
From and including 6th October, meetings will start at
7 p.m. The first hour will be devoted to morse classes.

The society will be operating a station as part of the Fourth ternational Jamboree-on-the-air. This is organised by the International Boy Scouts International Bureau and the station will be at the headquarters of the 3rd Mitcham Group on behalf of the Mitcham District Boy Scouts' Association. The Jamboree-on-the-air is to be held on October 20-22nd.

NORTHERN HEIGHTS AMATEUR RADIO SOCIETY Hon. Sec.: A. Robinson, G3MDW, Candy Cabin, Ogden, Halifax, Yorkshire.

Recent activities have included a spares sale and a film show. On October 4th G8CB gave a talk about "144 Mc/s". Meetings are held at the Sportsman Inn, Ogden, Halifax at 7.45 p.m. Future Event:

October 18th-Ragchew Night.

REPORTS OF CURRENT ACTIVITIES

SUTTON COLDFIELD RADIO SOCIETY Hon. Sec.: L. E. R. Hall, G3IGI, 24 Calthorpe Road, Walsall. Maurice Capewell, the vice-chairman of the society, is leaving the district to take a teaching appointment in Cheshire. Future Events:

October 26th-"DX TV Reception"; a tape recorded lecture by Charles Rafarel. November 9th-"G.D.O.-its construction and use"; by P.

Darragh.

November 23rd-The Fourth Annual General Meeting.

TEES-SIDE AMATEUR RADIO CLUB
Hon. Sec.: A. L. Taylor, G3JMO, 12 Endsleigh Drive, Acklam,
Middlesbrough, Yorkshire.

The most important event in the club's programme in the next few months, is the Annual Dinner. This year it will take place on Saturday, December 9th at 8 p.m. at the Corporation Hotel, Corporation Road Middlesbrough. The club meets fortnightly Settlement House, 132 Newport Road, Middlesbrough on Fridays at 8 p.m.

COURSES OF INSTRUCTION

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J. M. Falconer is giving a series of lectures entitled "Introduction Electronics: Its Principles and Applications" on Wednesdays, to Electronics: The first part of this series is to give the student the y p.m. The first part of this series is to give the student the simple principles of electronics. The latter part will be devoted to applications of electronics. The treatment of all subjects will be non-mathematical and no previous knowledge of electronics will be assumed. The course will be illustrated with films and demonstrated with the films a be assumed. The course will be illustrated with films and demon-strations, and some practical work may be undertaken by students.

High Gain Amplifier

(Continued from page 614)

together with the mains transformer, valveholders, smoothing choke, the controls and the jack sockets. A point to note is that the low impedance input jack socket must be insulated from the chassis, since neither side of the low impedance input is connected to earth. In the prototype, this insulation was effected using a rubber grommet (see Fig. 4). An alternative method would be to mount the socket on a piece of paxolin or other insulating material, and to bolt this to the chassis, taking care that no part of the jack socket touched the metal of the chassis. Having mounted the above-mentioned components, the heater wiring should be completed. This takes the form of a pair of wires, twisted tightly together, and pressed hard against the chassis. One side of the heater wiring should be earthed. The earth bus-bar is then fixed in position.

No special precautions need be taken when wiring the amplifier, other than the fact that all connections should be kept short, and that any earth connection which may be required should be made to the earth bus-bar, and not directly to the chassis. Screened leads should be used where they are indicated in the circuit diagram (Fig. 1).

Output Sockets

In the prototype amplifier, the output was taken via a coaxial plug and socket, and coaxial cable. There is no reason, however, why any other form of socket may not be used. Since one side of the output is earthed, then a normal jack socket bolted directly to the chassis may also be used.



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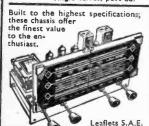
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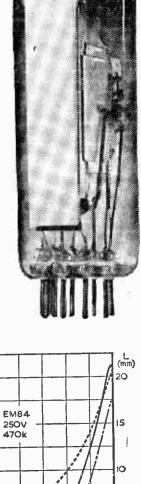
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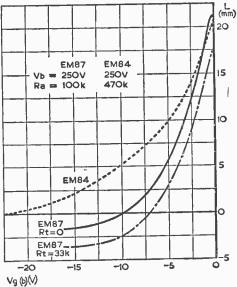
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The EM87

A new recording level indicator

(from "Mullard Outlook," September, 1961 issue)



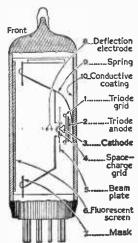


N many present-day tape recorders, the recording output available for driving the voltage-level indicator is about 10V, which is often insufficient to close the display of existing types of indicator. For this reason, Mullard have designed a new indicator—the EM87—which has a grid base of only 10V.

An additional feature of the EM87 is that a recording signal greater than 10V will cause the luminous areas of the display to overlap, thus giving a brighter section at the centre of the display. These large

display. These large voltages can result in distorted recordings, and the brighter section of the display thus serves as a useful indication of when the recording signal modulation is excession

These features are illustrated in Fig. 1, in which the control characteristic of the EM87 is shown. The intersection of the full curve with the horizontal axis shows the control-grid voltage at which the separation L between the luminous areas of the display is zero-that is, the voltage at which the closes.



display Fig. 2.—The construction of the EM87.

The excursion of the line below the horizontal axis indicates the overlapping of the luminous areas at recording signals in excess of 10V. At a target voltage of 250, the overlap will be 1.5mm for an input of 15V.

The broken line in Fig. 1 is the control characteristic of the EM84—the previously recommended Mullard voltage indicator. The grid base of this type is seen to be 22V.

Construction

The electrode structure of the new valve is shown in Fig. 2. The triode section is to the rear of the cathode, and the indicator section is in front of it.

The specially shaped cathode (3), 10mm long and coated on both surfaces, is mounted horizontally between two micas. Behind the cathode is the grid (1) and anode (2) of the triode section. A space-charge grid (4) is mounted immediately in front of the cathode, and is connected to the cathode. The space charge formed at this grid promotes a more uniform flow of electrons to the fluorescent screen or target (6). Next to the grid, and also maintained at cathode potential, is the beam plate (5). A slit in this plate ensures that the edges of the fluorescent display are sharp.

Fig. 1—Control characteristics: variations of display lengths with control grid voltage.

The deflection electrode (8) is situated in front of the slit in the beam plate. This electrode consists of two horizontal rods which are taken out

to a base pin.

The mask (7), which is normally connected to the H.T. line, serves to limit the size of the display on the fluorescent screen. A spring (9) on the mask assembly makes contact with a conductive coating (10) of stannic oxide on the inside of the bulb, and this coating is in contact with the fluorescent screen.

Operation

In a typical circuit (see Fig. 3) the deflection electrode is connected directly to the anode of the triode. With no signal, the current in the triode load is large, and the voltage of the deflection electrode is therefore about 50. The electrode is

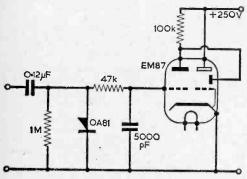


Fig. 3.—A typical circuit for the EM87.

thus about 200V negative with respect to the screen, which is at the H.T. line voltage. The electron beam is thus caused to diverge widely,

and the display is fully open.

When a signal is applied to the triode grid, the load current falls, the anode voltage rises, and the deflection electrode becomes less negative with respect to the screen. The divergence of the beam is therefore less, and the display is partially closed. When the input is 10V, the display is fully closed.

Load Resistance

The deflection-electrode potential of the EM87 is always positive, so that part of the electron stream to the target is intercepted by it and forms the deflection-electrode current. Thus, the current flowing in the load resistor in Fig. 3 has two parts: the anode current of the triode section, and the deflection-electrode current. The ratio of these two parts depends on the value of the load resistance used—the higher the resistance the greater the contribution of the deflection-electrode current, and hence the greater the dependence of the closing voltage on this part.

The electron beam impinging on the deflection electrode gives rise to secondary-emission electrons, and at certain voltages, some of these travel from the electrode to the target, thus reducing the deflection-electrode current. Because of this dependence on secondary emission, the current/voltage characteristic of the deflection electrode

will vary considerably from one EM87 to another. Thus in Fig. 3, if the load current contains a high proportion of deflection-electrode current, the closing voltage may be quite different for different EM87.

To reduce this variation in closing voltage, it is necessary therefore to reduce its dependence on the deflection-electrode part of the load current, and for this reason, the EM87 is designed for operation with a load resistance of only 100k. With this value, the anode-current part of the load current at the closing point is several times as great as the deflection-electrode component. The closing voltage is thus determined primarily by the triode characteristics of the EM87, and will change very little from valve to valve.

The low value of load resistance necessitates high values of amplification factor and mutual conductance in the triode section of the valve to produce sufficient voltage gain to drive the indicator section. The amplification factor of the EM87 is about four times that of the EM84 (which was designed to operate with a load resistance of 470k) and the mutual conductance is about 1.5 times

as large.

Increased Sensitivity

A typical circuit for the EM87 is given in Fig. 3. With the circuit values given in the figure, the display of the EM87 closes with a peak input of 10V, and an overlap in the display of 1.5mm occurs at

an input of 15V.

The target voltage in Fig. 3 is 250. A shorter grid base can be obtained if the target voltage is reduced by connecting a resistor in series with the target. This therefore provides a simple means of increasing the sensitivity of the EM87. The effect of including a 33k resistor between the target and the H.T. line is shown as the chain-dotted line in Fig. 1. The closing voltage is reduced to approximately 7, and a greater overlap for voltages greater than this is indicated.

A reduction in target voltage results in a loss of brightness. With the reduction obtained with the 33k resistor, the loss of brightness is not serious, but to maintain a satisfactory level of brightness, the target voltage should not be reduced below

170.

Other methods of increasing the sensitivity of the EM87 are possible, but these necessarily sacrifice qualities of the valve such as the sharpness of the display, or involve greater complexity of the circuit. However, when used in the simple circuit of Fig. 3, the new voltage-level indicator will fulfil the sensitivity requirements of most present-day tape records, and give also the facility of an indication of signal over-loading.

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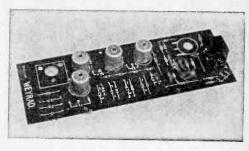
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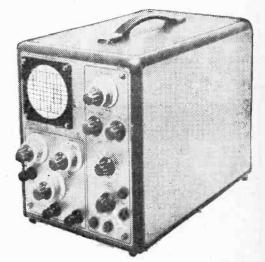
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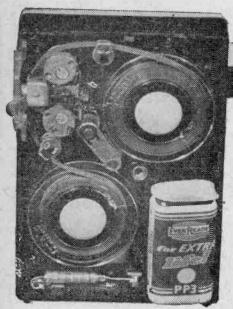
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The Memo-Cord costs 25 guineas complete with tape and case. It is made by Stuzzi Recording Devices Limited, 44 Southern Row, Kensington, London, W.10.



This resistance decade unit is made by the Bristol Electronic and Light Engineering Co.



The Stuzzi Memo-Cord.

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A NEW insulator tester—model 130C—has been released by Taylor Electrical Instruments Ltd. The model 130C covers a wide range of resistance readings and enables tests to be made on all types of component. The total resistance measurements covered are from 20Ω to 1,000M.

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It is designed to operate from an A.C. mains supply between 110V and 240V, 40 to 60c/s. The model 130C insulation tester is made by Taylor Electrical Instruments Ltd., Montrose Avenue, Slough, Buckinghamshire,



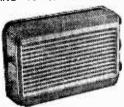
An insulation tester made by Taylor Electrical Instruments Ltd.

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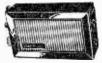
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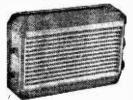
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OZ4A	5/6	6C4	918	128A7		CL33		FC13 KT3	15/-		gham 8403
114		6C5		128H7		CY31		KT36	27/6	Head Office and Warehouse: 14 SOUTH WH	IARF ROAD, W.2. Ter. AMB 0151/2, 0677.
1LD5		6CII6		128K7		DAF91		K . 81	17/-	Please send all correspondence ar	id Mail Orders to the Head Office.
1LN5		6D6		128L70			7/6	MH4	5/-	Modelmakers' Motors	I VENNER TIME SWITCHES
1R4 1R5		6F6 6F8G		128R7 12Y4		DCC90 DF91		MLS	8/-	Reversible 12V miniature motors; output	Eight-day clockwork type. One make and
194		6F33		13D1		DF92		NGT1 PCC84	3/6	5 watte at 7000 r.p.m. Dimensions 18in.	one break every 24 hours. 1 amp. 250V
185	6/-			25L6G7		DF96		PCL82		long x 1 in. dia. Shaft 0.077in. dia. x 4in.	contacts. Dial graduated in house Second
1T4	4/-	6116	1/6			DK63	6/-	PCL83	10/-	long. Centre-off reversing switch integral	hand, guaranteed, complete 27/6p. & p. with key.
1U5		6J5 6J6		39/44		DK91	6/-	PCL84		with the motor. Self-lubricat- ing sintered bronze bearings. 15/6 free.	
122		6K7	4/-	42		DK92 DK96		PCF80 PL36			MEADSETS
2C26A		6L6	9/-	83		DL33	7/-	PLSI	11/-	RELAYS	DLR-5 10/-
2C34	4/6	6L6G	7/-	83V	9/-	DL92	5/-	PL32	8/6	Second hand, guaranteed	HS-30/U 15/- Post and packing 1/9 per headset.
2D21 2E26		6L7		85 A1		DL93	5/-	PT15	10/-	S.T.C. MIDGET RELAYS:	Tost and packing 1/9 per headnet.
2K26		6N7 68A7	8/-	85 A2 717 A		DL94 DL95		PY81 PY82	7/6	1 M. Contact at 5A, 250 Ω Coil.	MAINS ENERGISED
344		68H7		807		DL96		PX25	10/-	Operating 40mA. Release 15mA 6/6 2 C.O. Bifurcated Contacts at	
3A5		68J7	5/-	814	35/-	DLS10	4/-	OS95/1	0 4/8	500mA, 700 Coil: operating	6in., 68Ω Fd., 5Ω Sp. Coil 8/-
3D6	4/-	68K7	5/6	815		EA76	7/6	QVD4-	7 12/6	16mA; release 5mA	10in., 68 Ω Fd., 5 Ω Sp. Coll 12/6
3Q4 394	5/-	681.7GT 68N7GT	6/8	832		EABC91		TTI1	3/-	SIGMA TYPE 4Cl or ALLIED TYPE "G"	Packing and postage 2/6 per speaker.
3V4		6887		955	3/-			U29	35/~ 8/6	High speed. 1B contact, 5000 Ω coii: current 4mA ± 5mA. Will	MAINS TRANSFORMERS
		6V6GT		958A		EC91	3/-	U25	12/6	operate with change of current of	Input 120V, output 6.3V at 5A,
5U4G	5/-	6X4		2051		ECC32		U26	9/6	0.2mA 5/8	7.5A and 0.5A, new 12/6 Input 120V, output 6.3V at 10A, 0.5A
5V4G 5Y3G		6X5GT 6Y6G		5670 5678		ECC81 ECC82		UF80	7/6	SIEMENS HIGH SPEED, SEALED	and 0.3A and 5V at 4A, new 15/-
5Z3		6Z4		5702		ECC83		UL84 VH54	1/6	1 C.O. contact at 500mA. Twin coil 2 x 140 Ω: operating 15mA with coils	Input 100/250V, output 275-0-275V
524	9/-	7AG7		5763		ECC84		VR56	4/8	in series, 30mA with coils parallel 5/-	at 80mA, 6.3V at 2.5A, and 0.6A 15/-
5Z4G	7/-	7F7		6005		ECC85	8/-	VH65	4/-	POST OFFICE RELAYS	Input 200-250V, Gardner or Parmeko, output 350-0-350V at 70mA D.C.,
6AB7 6AG5		7N7 7O7		7193		ECC91		VH75-		Type 600, 600 Ω coil, 2 C.O. contacts 6/6	and 6.3V at 2X1A and 2X3A, new 25/-
6AG7	7/6	724		7475 9002		ECF80 ECF82	10/6	T DOO	10/-	Type 3000, 500 Ω coil, 2C.O. contacts 7/8 Type 3000, 100 Ω coil, 4M-4B con-	Postage and packing 3/6 per transformer.
6AK5	5/-	11E3		9003	6/+	ECH35	8/-	VR100	6/-	tacts, break before make, Operating	AVOMETER MODEL 7
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6AT6	5/-	12AX7	7/-	ATP4	5/-	EF55	5/-	VE150	-30	RELAY	T36EHT45 Tubuiar, screw terminals, 1220V rms at 2mA, new 7/6
6AU6 6B4G	10/-	12AY7 12C8	10/-	AW2		EF80 EF86	6/-	TIT : OC	5/6	1 C.O.; twin 1450 Q coil and soaking	36EHT45, as above, but solder tag
6B8		1216	2/-	AW6		EF91		VU39 VU120	4/6	winding of 90 2. Speed of operation 500 or more per second. Complete	terminals 5/2
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Improving Selectivity

By P. McGoldrick

HE idea of the "Q" Multiplier was brought into this country from the United States several years ago. Briefly, it boosts the "Q" of a tuned circuit many times beyond its normal value. It is in this condition that it can reject or amplify a narro." frequency bandwidth. The valve "Q" multiplier usually employs a 12AU7 (ECC82) or 12AX7 (ECC83), and many variations of circuitry are obtainable. One example is shown in Fig. 1. This article describes a transistor unit, which makes use of the very cheap "white-spot" transistor (an OC45 or an XA103 may be used if one is available).

Theory and Practice (see Fig. 2)

Parallel-tuned circuits have been used for many years as trap circuits. Increasing the "Q" of the trap circuit reduces the width of the rejection notch. The transistorised "Q" multiplier makes use of this effect for its operation. A tuned circuit is made regenerative to increase its "Q" and is coupled to the I.F. stage of a receiver. By

changing the frequency of the regenerative circuit (C4) the frequency of the unit, found by the formula $F = \frac{1}{2}\pi\sqrt{LC}$ (where L is the inductance of the primary of the first I.F. transformer), the sharp notch can be moved about the passband of the receiver. The width of the notch is changed by controlling the amount of regeneration (R2). Regeneration is controlled by varying the D.C. operating voltage through the dropping resistors R1 and R2.

Construction

The original intention was to put the power supply in the same box as the unit. It was found, however, that the battery could make the box sideheavy, and so give it a tendency to fall over. Therefore it was decided to stand the battery behind the unit. The unit was originally built in a box which measured 4½in. x 3½in. x 2in., and provided ample room.

The only fixtures to be made are the tuning condenser, the regeneration control, and a central group board (one of the fixing bolts to be made a common earth). There are also two ½in, holes to be drilled on the side of the box opposite the control panel, which are for grommets and through which the connections to the

receiver and to the battery are made. The ImH coil is not critical, and in the author's unit an old "19" set coil, which read 1.2mH on an inductance bridge, was used. However, if such a meter is unavailable some firms market R.F. chokes rated at 0.8mH which are quite adequate for its purpose and are cheap.

Power is obtained from a 7½V battery which has non-reversible connections, and so far the drain on the battery has never exceeded 0.3mA.

The connection to the receiver is made by any sort of shielded or coaxial cable, and it is made across the primary of the first I.F. transformer.

The transistor should be soldered in last, and to prevent heat damage to it the usual heat dissipation rules should be adhered to.

Operation

When the unit has been completely wired (and double-checked), the battery is connected (making sure the poles of the battery are properly connected). The unit is then joined to the receiver.

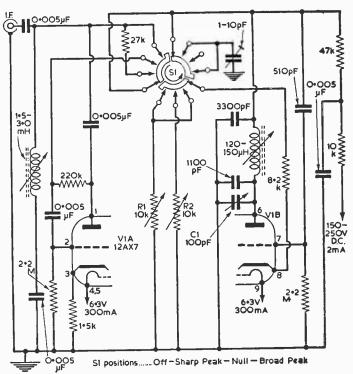
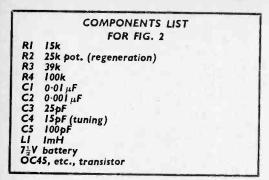


Fig. 1.—A valve "Q" multiplier; C1—tuning, R1—peak adjustment, R2—null adjustment.



When off, it should not affect receiver performance. When switched on, with the receiver set to a clear spot, the BFO to the centre of the pass-band and the tuning condenser and the regeneration control advanced to about half-way, a beat note should be heard from the receiver. If this is not heard at the central capacity of the tuning control, but in another position, the value of C5 should be adjusted accordingly.

To make the final alignment, the aerial should first be removed from the receiver, which is tuned to a broadcast station. With the BFO beating with the incoming signal, it will produce an audio tone. Adjust the BFO for a tone of about 1kc/s. Back off the control R2 until the oscillator becomes regenerative by alternately adjusting the tuning control C4 and the regeneration control R2 until a point can be found where the audio tone disappears, or at least is attenuated.

If, by any chance, a super-active "white-spot" transistor is used (or OC45 or XA103) and the

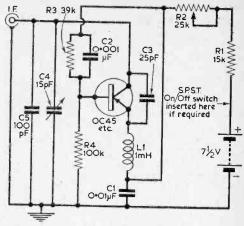


Fig. 2.—A transistorised "Q" multiplier.

regeneration control does not have the range to stop oscillator action, the value of R1 should be increased. Also, if the transistor does not appear to oscillate, then the value of R1 should be decreased.

Practice with the controls will produce better results, and it will be found after a while which are the ideal positions of the regeneration control to produce the best null, and the best peak.

This unit will increase the selectivity of any short-wave receiver, and will, at low cost, add immeasurably to the pleasure of amateur radio, especially on the reception of single side band.

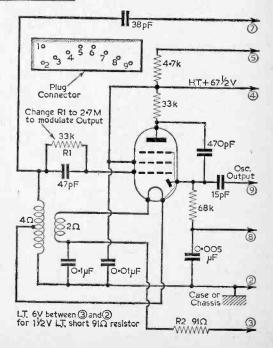
465kc/s SIGNAL GENERATOR **USING BFO UNIT ZA30038**

THIS ex-Government unit which measures only 2½in. x 4½in. x 1in., can be easily modified to a signal generator providing the usual I.F. of 465-470kc/s simply by changing R1 (33k) to 2.7M ½W. The unit as found in local radio component shops is ready for use and employs a single valve (IS5). The H.T. supply required is between 60 and 90V D.C. and the L.T. 6.3V D.C., but for convenience R2 (910) can be shorted out and L.T. is then 1.4V. A battery giving 69V + 1½V is the most convenient source of H.T. and L.T. and can be strapped to the unit with adhesive tape.

A short length of coaxial cable is joined to pins 9 and 2, the centre wire to pin 9 and the braiding to pin 2. The crocodile clips are joined to the other end for use on the radio to be lined up.

The other connections required are H.T.+ to pin 4; H.T.- to pin 2; L.T.+ to pin 3; L.T.to pin 2.

Fig. 1.—The circuit and plug connections of BFO Unit ZA30038.



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THE P.W. SIGNAL GENERATOR

THE CALIBRATION OF THE R.F. AND A.F. GENERATORS

By E. V. King

(Continued from page 518 of the October issue)

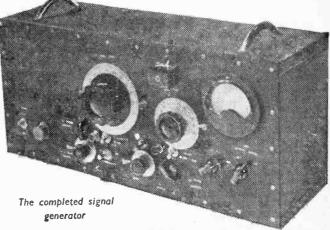
BEFORE the R.F. unit can be used for aligning receivers and similar purposes, it is necessary to calibrate it so that the frequencies corresponding to the settings of the tuning dial on the generator are known accurately. The way in which this signal generator will be calibrated is by preparing four graphs in which dial rotation is plotted against frequency for each of the four ranges.

Calibration of Range 1-150kc/s to 700kc/s

Set up the generator and a receiver as shown in Fig. 39. Switch on the R.F. unit (Chassis No. 2) and the Crystal Check Oscillator Unit (Chassis No. 4), for 20 minutes before beginning the calibration, so that the two units

20 minutes before beginning the calibration, so that the two units have time to reach their operating temperature.

1. Tune in the L.W. Light programme on the receiver (1500m). Remove the Aerial lead and retune the receiver slightly, if necessary, until the crystal "note" is heard, to verify that the crystal



2. Switch off the crystal oscillator and retune the receiver to the Light programme, and, with the R.F. range switch at position 1, and the output control full on, rotate the main frequency dial. Note the point at which the loudest heterodyne whistle is heard—this is where the crystal oscilla-

tor beats with the Light programme on 200kc/s. The dial reading for this position is then noted accurately.

3. Switch on the crystal oscillotor and the receiver. Now rotate the dial of the receiver towards the longer wavelengths until the next "note" from the crystal is heard — this will be 100kc/s further on and another heterodyne will be heard on rotating the tuning dial of the generator. This dial reading—the 300kc/s point—should be noted accurately.

4. Repeat (3) above and note the dial reading corresponding to 400kc/s (provided that the receiver will tune to this frequency).

5. Retune the receiver and the generator to the Light programme. Then, switch the Crystal Check Oscillator to the 10kc/s position. Now, as the dial of the generator is moved towards the 300kc/s point, from the 200kc/s point, a "swish"

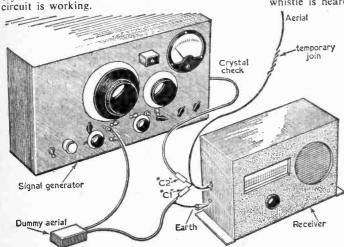


Fig. 39.—The method of interconnecting the R.F. generator and a receiver for the calibration procedure. (C1 and C2 are 2—500pF; the modulator should be switched off the crystal check oscillator to '100kc/s' and the R.F. generator to Range 1.)

will be heard every 10kc/s and these points can be noted to give more accurate calibration. When the operation is finished, a set of frequencies will have been obtained together with their corresponding dial positions. These values can now be transferred to a graph similar to Fig. 40 (larger in size, of course). To make the graph, a large sheet of squared paper (graph paper) is used. It is arranged with the longest side horizontal, and regular divisions are marked off along the bottom to represent increase in frequency of 100kc/s. The dial readings are similarly marked off on the left-hand side of the squared paper. The readings and values noted during the calibration are then transferred to the squared paper. example, in Fig. 40, the Light programme point was marked by putting a dot at the position corresponding to the frequency of 200kc/s and a dial reading of 74. Dots are made for all of the dial readings that were taken. Finally, the row of dots is inspected and it should

be found that they lie on a smooth curve. If any of the dots appear to be odd, or out of place, then the point corresponding to that dot should be checked.

A curve can now be drawn to link up the dots—it should be made a smooth curve, and it may be that some of the dots are to one side of the curve and some to the other. The aim should be to draw the curve so that about the same number of dots are on each side of it. If calibration has been carried out accurately, most of the dots

should fall very near to the curve.

At the lowest and highest frequencies, it was probably not possible to tune the receiver to hear the beats between the crystal oscillator and the R.F. unit. However, by noting the shape of the curve, it can be extended to cover these frequencies. The graph in Fig. 40 has been extended in this way.

Calibration of Range 2-600kc/s to 2.5Mc/s

1. Switch the receiver to the Medium Wave hand. Tune it to the Light programme on 12Mc/s. (If reception of this station is poor, then another will have to be used. The frequencies of local stations can be obtained from the local edition of the "Radio Times".) Switch the R.F. generator to Range 2 and turn the tuning control to the loudest heterodyne; the unit will now be set to 1.2Mc/s or the frequency of the station used.

2. Switch on the crystal check oscillator and tune the receiver towards the longer wavelengths until the crystal "note" is heard. The receiver will now be tuned to 1Mc/s, or to the nearest multiple of 100kc/s lower in frequency than the station to which the receiver was tuned. The generator can then be set to this frequency. The receiver can

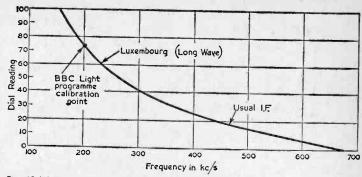
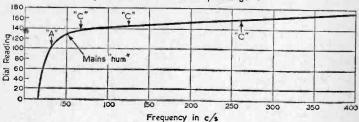


Fig. 40 (above).—The type of curve produced during the calibration (the results for Range I are illustrated above).

Fig. 41 (below).—The type of curve obtained during the calibration of the A.F. generator, in this instance for Range 1.



then be tuned to the next crystal marker—up or down in frequency—and the dial position on the generator noted for this frequency.

3. A set of readings of the dial should now be made similar to those obtained for Range I, but every 100kc/s instead of every 10kc/s—the 10kc/s points would come very close together and it would be very difficult to take readings.

4. Construct a graph similar to the one made for the first range. When the graph is finished, it can be checked by tuning the receiver to a station of which the frequency is known, and tuning the generator to the setting indicated by the graph. If the graph is correct, then a heterodyne should be heard between the station and the generator.

Calibration of Range 3-1-9Mc/s to 8-5Mc/s

This will be somewhat more difficult than the previous two ranges. The easiest way is to pick up an Amateur on the 40m band (on a Sunday morning) and take the frequency as 7Mc/s. Alternatively, a broadcasting station of known frequency can be used. In the same way as for the other two ranges, calibration points can be made every 100kc/s, but these points will be very close together. Another method would be to pick up stations of known frequency and use the dial readings to make up the graph.

Calibration of Range 4-4.5Mc/s to 20Mc/s

This will prove even more difficult than Range 3. The only practicable way is to use known stations for making the graph—the crystal check points will be very close together, and some of them will be very weak.

(Continued on page 650)

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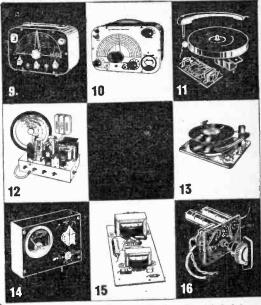
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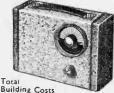
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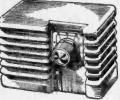
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transmitter was originally built for demonstration purposes—to show that a transmitter need not be elaborate. The power supply was obtained from a straightforward power unit, the total power requirements being only 40mA at 300V D.C. and less than 1A at 6·3V A.C. The R.F. power output is not great, being of the order of 2W; this power is sufficient for local contacts up to a range of about 7 miles or

The transmitter is designed to operate in the 7Mc/s band on C.W. or 'phone but, with a little modification, the output may be modified for C.W. in the 14Mc/s band with very little change in output power.

The Circuit (Fig. 1)

The R.F. oscillator is crystal controlled and although this results in a loss of flexibility of operation, crystal control has the twin advantages of stability and

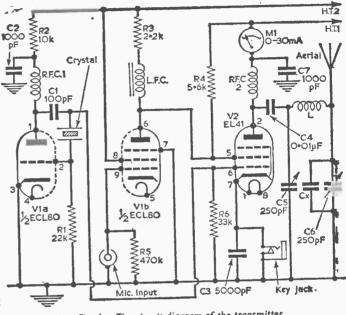


Fig. 1.—The circuit diagram of the transmitter.

Connecting plug Earth and (viewed on pins) 6.3V heater D.P.S.T. MMM. On/Off R7 10k 5W 5V S 6.3V heater switch HT.1 250 L.F. choke AC **V3** mains **C**9 **C**8 25C 603V heaters

cheapness over the variable frequency oscillator, besides which the crystal controlled oscillator is much more easily constructed and is very easy to set up. The oscillator is constructed around the triode section of an ECL80 (see Fig. 1), there being nothing original about the circuit. The oscillator output is taken to the grid of the output stage from the anode end of the crystal.

The modulation stage consists of the "other half" of the ECL80. This is used in conventional mode save for the A.F. choke in the anode circuit. It will be seen that screen series modulation is employed and as a result of this the anode of the pentode section of the ECL80 is directly coupled to the screen of the P.A. stage. It will be found that the value of R4, which feeds the screen of the EL41, has an effect on the power output from the P.A. stage. However, a compromise has to be made since too low a value of R4 will result in distorted audio. Screen series modulation is employed to avoid the use of a modulation transformer. Any type of L.F. choke may be used in the anode circuit of the modulator, provided that it will carry the anode current (30mA), and is of sufficient inductance.

Fig. 2.—The circuit of the power supply.

Mains Transformer The P.A. stage is R.C. coupled to the R.F. generator by way of C1 and R6. The output from the final stage is coupled to the aerial by a π -network, this being the easiest circuit to set up and also a reasonably efficient output network. C6 tunes the aerial to the network; it may be found that C6 has insufficient capacity to tune into the aerial (this will especially be so if a long aerial is used), in which case a capacitor, Cx, should be wired in parallel with C6 to raise the capacitance of the circuit. A suggested value for Cx would be about 300 pF. The actual value will have to be found by experiment, as it will depend on the length and position of the aerial (see also the article "Calculating π -Networks" in the October issue).

Construction

"Old Hands" may find much to criticise in the layout of the unit. However, the layout adopted has the advantage that the various sections of the circuit may be constructed and tested individually, each section being tested before the next stage is carried out. This should be of considerable help to the constructor who has never made up a circuit of this type before. The constructional details, therefore, will be given in parts with testing instructions for each section.

I -Power Unit (Fig. 2).

The power unit is straightforward. As it is probable that the reader has a suitable power unit to, hand, the power requirements were outlined

earlier (page 641). For the constructor who does not have a suitable power unit, a circuit is given in Fig. 2. No constructional details are given as no complications should arise.

2-R.F. Oscillator

The transmitter is made up on a chassis 7½in. x 3½in. x 2in. deep. The main holes to be made are shown in Fig. 3. The remainder of the holes to be drilled will depend upon the physical size of the components used. Holes for all the major components should be drilled to prevent the damage to components and wiring which would occur if chassis drilling were carried out at a later stage. The theoretical circuit for the R.F. oscillator is shown in Fig. 1 and a suggested wiring diagram shown in Fig. 4. In wiring this and all subsequent stages it is preferable to keep the wiring as short as possible. If the wiring diagrams are followed, no difficulty should be experienced.

Testing

Having checked connections for dry joints, etc., the unit should be connected to the power supply and a milliameter placed in series with the H.T. supply. When the valve (ECL80) has warmed up it should be found that the current reading on the milliameter is of the order of 10mA or so. If an unscreened aerial wire connected to an S.W. receiver tuned to the crystal fundamental is brought near to the valve or wiring of the oscillator stage,

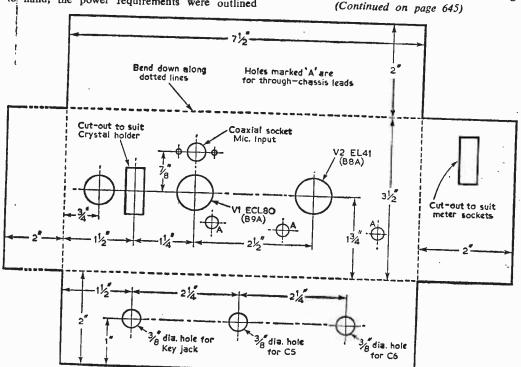


Fig. 3.—The chassis drilling details.

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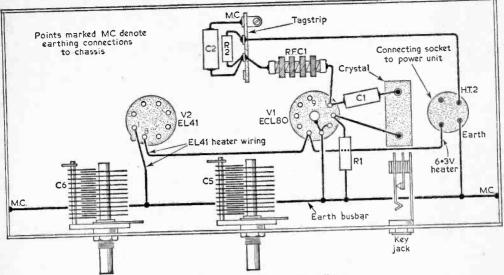


Fig. 4.—The wiring of the crystal oscillator.

(Continued from page 642)

the carrier will be detected by the set, and if the receiver is equipped with a BFO, a note will be heard. If the stage fails to oscillate, check the crystal by substitution.

3-The P.A. Stage

The P.A. or output stage is logically the next stage to wire. The wiring diagram is shown in Fig. 5. The switch in the cathode circuit can either be a switch proper or a closed circuit jack socket in order that the stage can be keyed for C.W. purposes. The condenser C3 across the switch

prevents key-clicks and was found to be indispensable in the original unit. The aerial coil (L) comprised in the original, 25 turns of 20s.w.g. enamelled copper wire wound on a 1½in. diameter former, each turn spaced from the next by a distance equal to the diameter of the wire (see Fig. 7).

Testing

Having checked the wiring thoroughly (in particular make sure that C1 has been connected to pin 6 of the EL41, and that the H.T. line is connected correctly), remove the milliammeter from the anode circuit of the R.F. oscillator and insert it in the anode circuit of the EL41.

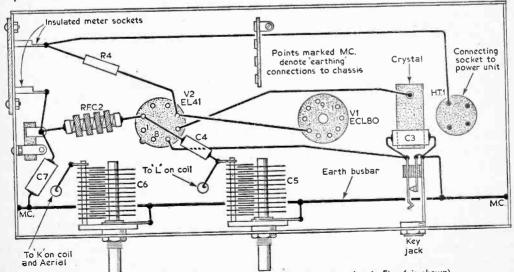


Fig. 5.—The wiring of the P.A. stage (only wiring additional to that in Fig. 4 is shown).

The power unit is then switched on and the milliameter should read between 10 and 30mA, depending on the state of the circuit. The aerial may then be connected to the coil. C5 should be adjusted so that the maximum current possible flows in the anode circuit. With the aerial con-

maximum dip occurs when the vanes of the capacitor are half closed. The H.T. current checks must, of course, be made with the cathode connected to the chassis. The final check of the output of the transmitter may be made by listening to the carrier on the S.W. receiver (if the set is

at all sensitive it is advisable to keep the R.F. gain low).

With these two stages complete, the set-up now comprises an keyed-carrier ordinary transmitter and it may be used as such. It must be emphasised that a Post-Office Transmitting Licence will be required before the operation and testing of this last stage. If the transmitter is to be used purely for C.W. and the modulator stage not used at all, it is advisable to strap the cathode, g1, g2 and g3 of the pentode section to earth and connect the anode to H.T.+ via a 47k resistor, The meter in the anode lead of the EL41 should be kept as a fixture and then a permanent check on transmitter efficiency is possible.

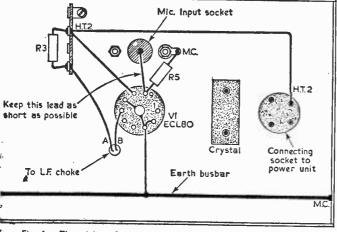


Fig. 6.—The wiring of the modulator stage (additional wiring only).

nected C6 should be adjusted so that the anode current "dips"—this dip can be as much as 20mA. If it is found that the dip is not great, or if no dip is shown, a capacitor of about 300pF should be wired across C6 (this new capacitor is Cx) and C6 again adjusted for maximum "dip". The value of Cx should be chosen so that

4—The Modulator

Fig. 6. The connection from the coaxial socket should be as short as possible to avoid hum. The input required for a reasonably modulated output is about \(\frac{1}{2}\) to 1V.

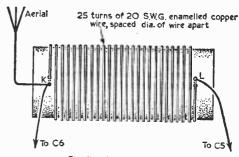
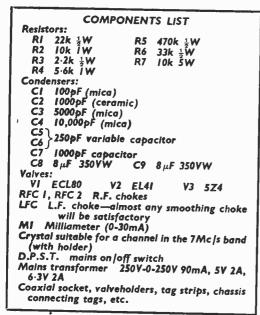


Fig. 7.—The tank coil.

The final testing must be carried out with the aid of a suitable receiver which can be tuned to the fundamental frequency of the transmitter, which should be modulated by a suitable source of A.F. and the receiver tuned to the transmitter. The quality of the modulation should be checked and the maximum possible modulation level used without distortion. The transmitter is now complete.

If it is required to use the transmitter in the 14Mc/s band, it will be found that it will cover this band if half of the turns on the coil are shorted out. It will be appreciated that it is only possible to use the transmitter for C.W. in this condition. Simple band switching may be accomplished by using a simple shorting switch.



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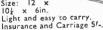


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Letters to the Editor

The Editor does not necessarily agree with the opinions expressed by his correspondents

Whilst we are always pleased to assist readers with their technical difficulties, we regret that we are unable to supply diagrams or provide instructions for modifying commerical or surplus equipment. We cannot supply alternative details for receivers described in these pages. WE CANNOT UNDERTAKE TO ANSWER QUERIES OVER THE TELE-PHONE. If a postal reply is required a stamped and addressed envelope must be enclosed with the coupon from page iii of the cover.

SWL AND HAMS

SIR,—With reference to E. L. W.'s letter in the September issue, I am sure that he must have caught the ham he visited at an inconvenient time or didn't have the right approach. I have always found them most friendly and helpful, and have obtained many useful tips from them. I advise E. L. W. to try again, he evidently caught the ham in a bad mood.—B. J. CHAPMAN (Birmingham).

SIR,—With reference to E. L. W.'s letter in which he complains of being badly received when visiting a local ham, I can assure him that most operators are willing to help SWLs with their weeklers.

At one time I was looking for a decent S.W. receiver so I went for some advice from a local ham. He was most helpful, and immediately found an advertisement for a set, the same as his own. I have since bought this receiver and its per-

formance is very satisfactory.
In my experience I have found all operators very helpful.—I. CATLEUGH (East Lothian, Scot-

TRANSMITTER LICENCES

land).

SIR,—I notice that once again the controversy about "low power transmitting" is rearing

Its head.

There is a solution to this problem which may be of interest to readers. By all means let those who wish to become genuine "hams" continue with the Radio Amateurs Exam and GPO morse test. On the other hand there is an easy way for others to enjoy using "speech only" equipment of a very the problem of the problem.

high standard, with no cost to themselves.

Any person over 18 years of age can join the Signal Section of the Civil Defence Corps. Here they will receive a thorough training in wireless procedure, maintenance of equipment, station siting and other relevant subjects.

All the wireless equipment used is VHF and ranges from walkie-talkies to 5 channel fixed mains sets.—G. D. THORNTON (Fife).

CORRESPONDENTS WANTED

SIR,—I am a regular reader of P.W. I am interested in radio technology and have started a radio repair shop of my own. I would

like to correspond with any radio technician from anywhere. I will answer all letters received promptly.—S. J. D. RODRIGO (Miriskotuwa, Kahagolla, Diyatalawa, Ceylon).

TRANSISTOR SET RECEPTION

SIR,—Mr. James appears to have been exceedingly unlucky in his choice of circuits. In his letter in the June issue he says that designers should state in what part of the country they have tested the set. I fully agree with this, but, that in itself will give no criterion as to the performance to be expected elsewhere. I feel that it is time a measurement test should be given, say so much output with so much input, or in other words a sensitivity rating such as the manufacturers give with their products.—G. BOOTH (Norwich).

BBC TV RECEPTION

SIR.—I notice that Mr. Bickham suggests that radiation from an I.F. stage may be the cause of listeners hearing television on the short waves (August issue). I do not agree. Truly, it may be radiated, but not from the I.F. stages. I think most receivers have AVC and other arrangements which would prevent this, and after all the I.F. transformers are invariably totally screened. No, I think the radiation comes from the output stages or at least somewhere in the audio section, where screening is not introduced. This was, in fact, often experenced by TV amateurs when ITV started and receivers were in use with straight circuits. This did not occur with the superhet, as the signal at the output stage was not at the signal frequency.—G. KIMBER (Manchester).

YOUNG ENTHUSIASTS

SIR,—On reading the letter by D. Hill of Edinburgh in your last issue I thought he would be interested to know that I received the same transmission on 14·3Mc/s on an ex-naval R1110

This transmission is also heard on the same frequency during the day.—V. J. Rowley (Plymouth).

SIR,—In the October edition of P.W., Mr. D. Hill requested information on a station announcing itself as "Rome Radio". I have myself received this particular station several times, at reasonable strength, between 27 and 29m, at all times of the day. The full announcement reads as follows: "This is Rome Radio, Maritime Radio Telephone Service. This is a test transmission for receiver adjustments."

Occasionally, on the same wavelength, a programme can be heard, so this station is presumably

a commercial broadcasting station.—B. Dempster (Mapperley).

SIR,—With reference to D. Hill's letter which appeared in your October issue, the transmission which he heard comes from a station situated near Rome, on the West Coast of Italy. The purpose of this station is to maintain a radiotelephone service with nearby ships. The recording which Mr. Hill heard is radiated when the radio-telephone service is not being used. The purpose of this is to enable the neighbouring ships to tune accurately to the station before calling. The recording goes as follows: "This is Rome Radio, Maritime Radio-Telephone Service. This is a test transmission for receiver adjustment purposes." This station operates on several frequencies but is usually heard at the H.F. end of the 19 and 16m band.—B. Pears (Rowlands Gill, Co. Durham).

[The above are only three of many letters received in reply to Mr. Hill's letter, and we thank all of the readers who went to the trouble of sending information. This is the true 'ham' spirit.—Editor.]

TRANSISTOR RADIO IN THE ALPS

SIR,—Some time ago I built a small reflex pocket receiver (with an earphone) and subsequently took it with me on my annual Continental tour. Most of the time I was on the high Alpine passes in several countries. I was surprised that radio reception was uniformly very bad, even with an external aerial. I did not receive any signals during day light hours but there was plenty of 60 cycle hum from the power transmission lines. Even after dark it was only possible to receive one or two stations, and these were of poor strength. The surrounding high peaks would, of course, act as barriers in some directions, but one would have expected good signals where there were no obstructions. In S.E. Austria, where the topography is comparable with England, I found reception to be quite normal. It would have been interesting to have tried the set on the Comet aircraft, but this was out of the question, as I read recently that the use by passengers of portable radios had interfered with the normal radio services of several planes.—F. CHURCHILL (War-

SHORT-WAVE SECTION

(Continued from page 621)

Performance

If the unit is used in the "reject" position with the frequency of maximum rejection at 2kc/s, frequencies of 1850c/s and 2150c/s will be reduced in amplitude by about eight times, whilst rejection of 2kc/s signals will be virtually complete. A frequency of 1500c/s would not be greatly attenuated. The width of the rejected band is proportional to the rejected frequency.

The input should always be less than 1V; overloading gives very poor results.

As an Oscillator

When the circuit is used as an oscillator, the regeneration control should be advanced just enough for oscillation to occur.

Power Supplies

The power requirements for either the circuit of Fig. 3 or that of Fig. 4 are 6.3V at 0.6A (or 12.6V at 0.3A) for the valve heaters and about 150V at a few mA for the H.T. This can easily be obtained from the power pack of almost any mains receiver which employs a 6.3V heater supply.

Construction

A sub-chassis of size 5in. x 4in. x 2½in. will easily accommodate the unit. The ganged frequency control, the regeneration control and the select/reject switch must, of course, be brought to the front panel of the receiver or of the unit if the latter is separated from the receiver. Leads should be reasonably short where possible, but any leads which must be more than a few inches long should be screened if they carry audio frequency currents. It is probably unwise to attempt to accomadate all of the elements of the select/reject switch on one wafer.

THE P.W. SIGNAL GENERATOR

(Continued from page 638)

Calibration of the A.F. Oscillator

The procedure for calibration of the audio generator is very similar to that for the R.F. generator; dial readings corresponding to known frequencies are noted, for each range, on a graph (see Fig. 41). Before actual calibration, the dial suggested (Bulgin 2/K402) has to be modified by extending the scale to 170°. This can be carried out with Indian ink, which is varnished when dry.

Procedure

Connect the output of the audio oscillator to a loudspeaker or amplifier and switch it to Range 1. To another loudspeaker, connect the 6.3V heater supply via a resistor of 1000\Omega (take care not to short-circuit the 6.3V supply). Tune the generator to "zero beat"—the point at which the two notes appear to merge. This will establish the 100c/s point. It should also be possible to establish the 150c/s and 200c/s points.

The use of a standard tuning fork will enable the frequency of 256c/s to be located (a C fork). For other frequencies, a piano can be used—Middle C will give about 260c/s, one octave lower giving 131c/s, the next 65c/s and the next 33c/s. Finally, a graph can be drawn of frequencies and dial readings.

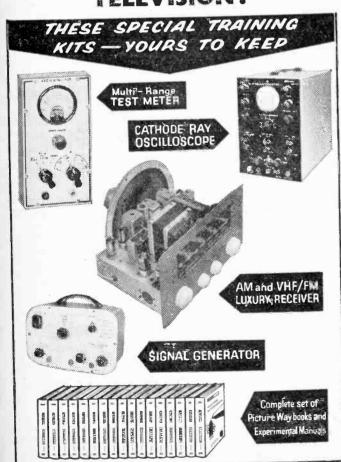
For Range 2, a piano can be used or the various tuning signals of the BBC—the one used early in the mornings, before programmes begin, is 1000c/s and the one before the Third programme and Network Three is 440c/s.

For Range 3, which is rather more difficult, a piano can be used for 2kc/s to 4kc/s (by a good musician). The graph will have to be drawn in by estimation for frequencies above about 15kc/s because many people cannot hear above this frequency.

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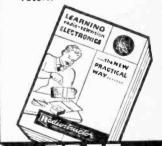
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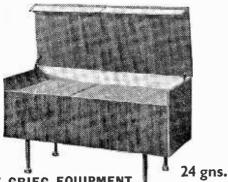
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The index letters which precede the Blueprint Number indicate the periodical in which the description appeared. Thus PW refers to PRACTICAL WIRELESS; AW to Amateur Wireless and WM to Wireless Magazine.

Send (preferably) a postal order to cover the cost of the Blueprint (stamps over 6d. unacceptable) to PRACTICAL WIRELESS, Blueprint Dept., George Newnes, Ltd., Tower House, Southampton Street, London, W.C.2.

SPECIAL NOTE

THE following blueprints include some pre-war designs and are kept in circulation for those constructors who wish to make use of old components which they may have in their spares box. The majority of the components for these receivers are no longer stocked by retailers.

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PRACTICAL WIRELESS, NOVEMBER, 19

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